

CHAPTER EIGHT

INTERCHANGES

The information contained in this chapter pertains to the design of ramp connections only. The designer should be familiar with Chapter 10 of the 2011. "A Policy on Geometric Design of Highways and Streets" before beginning the design of any interchange.

The configuration of an interchange should allow all movements to operate at an acceptable level of service as defined in the 1998 "Highway Capacity Manual". The Project Engineer should approve a preliminary design of the interchange before final surveys begin.

CONTROL OF ACCESS AT INTERCHANGES

Control of access along Y lines at interchanges is needed for a minimum of 1000' beyond the ramp intersections. If for some reason this is not practical, we should provide full control of access for 350' and then use a raised island to eliminate left turns for the remaining 650'.

LOOP DESIGN

8-1

TYPICAL SECTION:

2'-6" curb and gutter is placed on the inside of all loops. Pavement widths should be designed to meet Design Widths of Pavements for Turning Roadways see 8-1 Figure 1. Case II (Provision for passing a stalled vehicle).

LOOP DESIGN (continued)

8-1

DESIGN WIDTHS OF PAVEMENTS FOR TURNING ROADWAYS

8 - 1

F - 1

Design Widths of Pavements for Turning Roadways									
US Customary									
Radius on inner edge of pavement	Pavement Width (ft)								
	Case I			Case II			Case III		
	One-lane, one-way operation- -no provision for passing a stalled vehicle			One-lane, one-way operation- -with provision for passing a stalled vehicle			Two-lane operation--either one way or two way		
	Design traffic conditions								
R (ft)	A	B	C	A	B	C	A	B	C
50	18	18	23	20	26	30	31	36	45
75	16	17	20	19	23	27	29	33	38
100	15	16	18	18	22	25	28	31	35
150	14	15	17	18	21	23	26	29	32
200	13	15	16	17	20	22	26	28	30
300	13	15	15	17	20	22	25	28	29
400	13	15	15	17	19	21	25	27	28
500	12	15	15	17	19	21	25	27	28
Tangent	12	14	14	17	18	20	24	26	26
Width modification regarding edge treatment									
No stabilized shoulder	None			None			None		
Sloping curb	None			None			None		
Vertical curb: one side	Add 1 ft			None			Add 1 ft		
two sides	Add 2 ft			Add 1 ft			Add 2 ft		
Stabilized shoulder, one or both sides	Lane width for conditions B & C on tangent may be reduced to 12 ft where shoulder is 4 ft or wider			Deduct shoulder width; minimum pavement width as under Case I			Deduct 2 ft where shoulder is 4 ft or wider		

Note: A = predominantly P vehicles, but some consideration for SU trucks.
 B = sufficient SU vehicles to govern design, but some consideration for semitrailer combination trucks
 C = sufficient bus and combination-trucks to govern design

LOOP DESIGN (Continued)

8-1

SHOULDERS:

See Chapter 1-4D of this manual for width of usable shoulder on outside of loops.

ALIGNMENT:

Freeways - 150' to 250' radii unless conditions warrant otherwise. On interstate, loops should be designed for a 30 mph design speed where feasible. (230' radii minimum for 30 mph design speed).

Expressways - A 150' radius is acceptable on highways with a 50 mph or less design speed.

Appropriate deceleration and acceleration lanes should be provided for all loops. See Part 1, Section 8-7, Table 1 of this manual. For additional information, see A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (2011), ch. 10, for acceleration and deceleration lane lengths.

RAMP DESIGN

8-2

TYPICAL SECTION:

Pavement width is normally 14 feet, but where traffic volumes or truck percentages are high, the designer should consider using a width of 16 feet. On the interstate system, the pavement width should be 16 feet.

SHOULDERS:

See Chapter 1-4E of this manual for width of usable shoulder. Paved shoulders are required on both sides.

ALIGNMENT:

Ramp alignments should be designed to provide room for future loop placement in the quadrants where loops could be placed to eliminate left turns from the Y line onto the ramp. Use a minimum of 170' to 250' radii for the future loop. Accommodate for the future loop lane under the bridge as well.

RAMP DESIGN (continued)

8-2

Ramp design speeds should approximate the low volume running speed on the intersecting highways. This design speed is not always practicable and lower design speeds may be necessary.

GUIDE VALUES FOR RAMP DESIGN SPEED

8-3

GUIDE VALUES FOR
RAMP DESIGN SPEED AS RELATED TO HIGHWAY DESIGN SPEED

Highway design speed (mph)	30	35	40	45	50	55	60	65	70	75
Ramp design speed (mph)										
Upper range (85%)	25	30	35	40	45	48	50	55	60	65
Middle range (70%)	20	25	30	33	35	40	45	45	50	55
Lower range (50%)	15	18	20	23	25	28	30	30	35	40
Corresponding minimum radius (feet)	<u>See charts 8-3 C-1 Thru C-5</u>									

NOTE: Ramp design speeds above 30 mph seldom are applicable to loops. For highway design speeds of more than 50 mph, the loop design speed should not be less than 25 mph (150' radius). For additional information, see A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (2011), ch. 10.

Desirable curvatures for normal 50 mph design speeds in the vicinity of the gore areas are as follows:

Rural Exit	3 to 5 degrees
Rural Entrance	3 to 5 degrees
Urban Exit	4 to 6 degrees
Urban Entrance	3 to 6 degrees

CHART 1

US CUSTOMARY

C-1

e (%)	$V_d = 15$ mph R (ft)	$V_d = 20$ mph R (ft)	$V_d = 25$ mph R (ft)	$V_d = 30$ mph R (ft)	$V_d = 35$ mph R (ft)	$V_d = 40$ mph R (ft)	$V_d = 45$ mph R (ft)	$V_d = 50$ mph R (ft)	$V_d = 55$ mph R (ft)	$V_d = 60$ mph R (ft)
1.5	796	1410	2050	2830	3730	4770	5930	7220	8650	10300
2.0	506	902	1340	1880	2490	3220	4040	4940	5950	7080
2.2	399	723	1110	1580	2120	2760	3480	4280	5180	6190
2.4	271	513	838	1270	1760	2340	2980	3690	4500	5410
2.6	201	388	650	1000	1420	1930	2490	3130	3870	4700
2.8	157	308	524	817	1170	1620	2100	2660	3310	4060
3.0	127	251	433	681	982	1370	1800	2290	2860	3530
3.2	105	209	363	576	835	1180	1550	1980	2490	3090
3.4	88	175	307	490	714	1010	1340	1720	2170	2700
3.6	73	147	259	416	610	865	1150	1480	1880	2350
3.8	61	122	215	348	512	730	970	1260	1600	2010
4.0	42	86	154	250	371	533	711	926	1190	1500

Note: Use of $e_{\max} = 4\%$ should be limited to urban conditions.

Minimum Radii for Design Superelevation Rates, Design Speeds, and $e_{\max} = 4\%$

REV. DATE : 06/15/11

REVISION 7

CHART 2

US CUSTOMARY

C-2

e (%)	$V_d = 15$ mph R (ft)	$V_d = 20$ mph R (ft)	$V_d = 25$ mph R (ft)	$V_d = 30$ mph R (ft)	$V_d = 35$ mph R (ft)	$V_d = 40$ mph R (ft)	$V_d = 45$ mph R (ft)	$V_d = 50$ mph R (ft)	$V_d = 55$ mph R (ft)	$V_d = 60$ mph R (ft)	$V_d = 65$ mph R (ft)	$V_d = 70$ mph R (ft)	$V_d = 75$ mph R (ft)	$V_d = 80$ mph R (ft)
1.5	868	1580	2290	3130	4100	5230	6480	7870	9410	11100	12600	14100	15700	17400
2.0	614	1120	1630	2240	2950	3770	4680	5700	6820	8060	9130	10300	11500	12900
2.2	543	991	1450	2000	2630	3370	4190	5100	6110	7230	8200	9240	10400	11600
2.4	482	884	1300	1790	2380	3030	3770	4600	5520	6540	7430	8380	9420	10600
2.6	430	791	1170	1610	2130	2740	3420	4170	5020	5950	6770	7660	8620	9670
2.8	384	709	1050	1460	1930	2490	3110	3800	4580	5440	6200	7030	7930	8910
3.0	341	635	944	1320	1760	2270	2840	3480	4200	4990	5710	6490	7330	8260
3.2	300	566	850	1200	1600	2080	2600	3200	3860	4600	5280	6010	6810	7680
3.4	256	498	761	1080	1460	1900	2390	2940	3560	4250	4890	5580	6340	7180
3.6	209	422	673	972	1320	1740	2190	2710	3290	3940	4540	5210	5930	6720
3.8	176	358	583	864	1190	1590	2010	2490	3040	3650	4230	4860	5560	6320
4.0	151	309	511	766	1070	1440	1840	2300	2810	3390	3950	4550	5220	5950
4.2	131	270	452	684	960	1310	1680	2110	2590	3140	3680	4270	4810	5520
4.4	116	238	402	615	868	1190	1540	1940	2400	2920	3440	4010	4630	5220
4.6	102	212	360	555	788	1090	1410	1780	2210	2710	3220	3770	4380	5040
4.8	91	189	324	502	718	995	1300	1640	2050	2510	3000	3550	4140	4790
5.0	82	169	292	456	654	911	1190	1510	1890	2330	2800	3330	3910	4550
5.2	73	152	264	413	595	833	1090	1390	1750	2160	2610	3120	3690	4320
5.4	65	136	237	373	540	759	995	1280	1610	1990	2420	2910	3460	4090
5.6	58	121	212	335	487	687	903	1160	1470	1830	2230	2700	3230	3840
5.8	51	106	186	296	431	611	806	1040	1320	1650	2020	2460	2970	3560
6.0	39	81	144	231	340	485	643	833	1060	1330	1660	2040	2500	3050

Minimum Radii for Design Superelevation Rates, Design Speeds, and $e_{\max} = 6\%$

CHART 3

US CUSTOMARY

C-3

e (%)	$V_d = 15$ mph R (ft)	$V_d = 20$ mph R (ft)	$V_d = 25$ mph R (ft)	$V_d = 30$ mph R (ft)	$V_d = 35$ mph R (ft)	$V_d = 40$ mph R (ft)	$V_d = 45$ mph R (ft)	$V_d = 50$ mph R (ft)	$V_d = 55$ mph R (ft)	$V_d = 60$ mph R (ft)	$V_d = 65$ mph R (ft)	$V_d = 70$ mph R (ft)	$V_d = 75$ mph R (ft)	$V_d = 80$ mph R (ft)
1.5	932	1640	2370	3240	4260	5470	6710	8150	9720	11500	12900	14500	16100	17800
2.0	676	1190	1720	2370	3120	3970	4930	5990	7150	8440	9510	10700	12000	13300
2.2	605	1070	1550	2130	2780	3570	4440	5400	6450	7600	8600	9660	10800	12000
2.4	546	959	1400	1930	2540	3240	4030	4910	5870	6930	7830	8810	9850	11000
2.6	496	872	1280	1760	2320	2960	3690	4490	5370	6350	7180	8090	9050	10100
2.8	453	796	1170	1610	2130	2720	3390	4130	4950	5850	6630	7470	8370	9340
3.0	415	730	1070	1480	1960	2510	3130	3820	4580	5420	6140	6930	7780	8700
3.2	382	672	985	1370	1820	2330	2900	3550	4250	5040	5720	6460	7260	8130
3.4	352	620	911	1270	1690	2170	2700	3300	3970	4700	5350	6050	6800	7620
3.6	324	572	845	1180	1570	2020	2520	3090	3710	4400	5010	5680	6400	7180
3.8	300	530	784	1100	1470	1890	2360	2890	3480	4140	4710	5350	6030	6780
4.0	277	490	729	1030	1370	1770	2220	2720	3270	3890	4450	5050	5710	6420
4.2	255	453	678	955	1280	1680	2080	2560	3080	3670	4200	4780	5410	6080
4.4	235	418	630	893	1200	1560	1960	2410	2910	3470	3980	4540	5140	5800
4.6	215	384	585	834	1130	1470	1850	2280	2750	3290	3770	4310	4890	5530
4.8	193	349	542	779	1060	1390	1750	2160	2610	3120	3590	4100	4670	5280
5.0	172	314	499	717	991	1310	1650	2040	2470	2960	3410	3910	4460	5050
5.2	154	284	457	676	929	1230	1560	1930	2350	2820	3250	3740	4280	4840
5.4	139	258	420	627	870	1160	1480	1830	2230	2680	3110	3570	4080	4640
5.6	126	236	387	582	813	1090	1390	1740	2120	2560	2970	3420	3920	4460
5.8	115	216	358	542	761	1030	1320	1650	2010	2430	2840	3280	3760	4280
6.0	105	199	332	506	713	965	1250	1560	1920	2320	2710	3150	3620	4140
6.2	97	184	308	472	669	909	1180	1480	1820	2210	2600	3020	3460	3930
6.4	89	170	287	442	628	857	1110	1400	1730	2110	2490	2910	3360	3850
6.6	82	157	267	413	590	808	1050	1330	1650	2010	2380	2790	3240	3700
6.8	76	146	248	386	553	761	990	1260	1560	1910	2280	2690	3120	3600
7.0	70	135	231	360	518	716	933	1190	1480	1820	2180	2580	3010	3480
7.2	64	125	214	336	485	672	878	1120	1400	1720	2070	2470	2900	3370
7.4	59	115	198	312	451	628	822	1060	1320	1630	1970	2350	2780	3250
7.6	54	105	182	287	417	583	765	980	1230	1540	1850	2230	2650	3120
7.8	48	94	164	261	380	533	701	901	1140	1410	1720	2090	2500	2970
8.0	38	76	134	214	314	444	587	758	960	1200	1480	1810	2210	2670

Minimum Radii for Design Superelevation Rates, Design Speeds, and $e_{\max} = 8\%$ (Continued)

CHART 4

US CUSTOMARY

C-4

e (%)	$V_d = 15$ mph R (ft)	$V_d = 20$ mph R (ft)	$V_d = 25$ mph R (ft)	$V_d = 30$ mph R (ft)	$V_d = 35$ mph R (ft)	$V_d = 40$ mph R (ft)	$V_d = 45$ mph R (ft)	$V_d = 50$ mph R (ft)	$V_d = 55$ mph R (ft)	$V_d = 60$ mph R (ft)	$V_d = 65$ mph R (ft)	$V_d = 70$ mph R (ft)	$V_d = 75$ mph R (ft)	$V_d = 80$ mph R (ft)
1.5	947	1680	2420	3320	4350	5520	6830	8280	9890	11700	13700	14700	16300	18000
2.0	694	1230	1760	2440	3210	4080	5050	6130	7330	8630	9720	10900	12200	13500
2.2	625	1600	2200	2900	3680	4570	5540	6630	7810	9100	10200	11400	12700	14000
2.4	567	1010	1460	2000	2640	3350	4160	5050	6050	7130	8040	9010	10100	11200
2.6	517	1330	1840	2420	3080	3800	4640	5550	6550	7630	8790	9960	11200	12500
2.8	475	1230	1760	2420	3080	3800	4640	5550	6550	7630	8790	9960	11200	12500
3.0	438	1140	1600	2170	2830	3520	4280	5130	6050	7050	8130	9280	10500	11800
3.2	406	1050	1500	2060	2680	3370	4130	4980	5880	6880	7960	9130	10400	11800
3.4	377	970	1400	1920	2530	3200	3970	4780	5680	6680	7760	8930	10200	11600
3.6	352	913	1360	1860	2470	3140	3910	4720	5620	6620	7700	8870	10100	11500
3.8	329	856	1270	1770	2380	3050	3820	4630	5530	6530	7610	8780	10000	11400
4.0	308	804	1190	1660	2270	2940	3710	4520	5420	6420	7500	8670	9900	11300
4.2	289	756	1130	1600	2200	2870	3640	4450	5350	6350	7430	8600	9830	11200
4.4	271	713	1080	1560	2160	2830	3600	4410	5310	6310	7390	8560	9790	11100
4.6	255	673	1030	1520	2120	2790	3560	4370	5270	6270	7350	8520	9750	11000
4.8	240	636	1000	1490	2090	2760	3530	4340	5240	6240	7320	8490	9720	10900
5.0	226	601	960	1460	2060	2730	3500	4310	5210	6210	7290	8460	9690	10800
5.2	213	569	920	1430	2030	2700	3470	4280	5180	6180	7260	8430	9660	10700
5.4	200	539	881	1400	2000	2670	3440	4250	5150	6150	7230	8400	9630	10600
5.6	188	511	848	1370	1970	2640	3410	4220	5120	6120	7200	8370	9600	10500
5.8	176	484	809	1340	1940	2610	3380	4190	5090	6090	7170	8340	9570	10400
6.0	164	458	769	1310	1910	2580	3350	4160	5060	6060	7140	8310	9540	10300
6.2	152	433	728	1280	1880	2550	3320	4130	5030	6030	7110	8280	9510	10200
6.4	140	409	686	1250	1850	2520	3290	4100	5000	6000	7080	8250	9480	10100
6.6	130	386	645	1220	1820	2490	3260	4070	4970	5970	7050	8220	9450	10000
6.8	120	363	606	1190	1790	2460	3230	4040	4940	5940	7020	8190	9420	9900
7.0	112	343	569	1160	1760	2430	3200	4010	4910	5910	6990	8160	9390	9800
7.2	105	324	534	1130	1730	2400	3170	3980	4880	5880	6960	8130	9360	9700
7.4	98	306	500	1100	1700	2370	3140	3950	4850	5850	6930	8100	9330	9600
7.6	92	290	467	1070	1670	2340	3110	3920	4820	5820	6900	8070	9300	9500
7.8	86	274	437	1040	1640	2310	3080	3890	4790	5790	6870	8040	9270	9400
8.0	81	260	408	1010	1610	2280	3050	3860	4760	5760	6840	8010	9240	9300
8.2	76	246	377	980	1580	2250	3020	3830	4730	5730	6810	7980	9210	9200
8.4	72	234	359	950	1550	2220	2990	3800	4700	5700	6780	7950	9180	9100
8.6	68	221	341	920	1520	2190	2960	3770	4670	5670	6750	7920	9150	9000
8.8	64	209	324	890	1490	2160	2930	3740	4640	5640	6720	7890	9120	8900
9.0	60	198	307	860	1460	2130	2900	3710	4610	5610	6690	7860	9090	8800
9.2	56	186	291	830	1430	2100	2870	3680	4580	5580	6660	7830	9060	8700
9.4	52	175	274	800	1400	2070	2840	3650	4550	5550	6630	7800	9030	8600
9.6	48	163	256	770	1370	2040	2810	3620	4520	5520	6600	7770	9000	8500
9.8	44	150	238	740	1340	2010	2780	3590	4490	5490	6570	7740	8970	8400
10.0	36	126	200	690	1290	1960	2750	3560	4470	5470	6550	7710	8930	8300

Minimum Radii for Design Superelevation Rates, Design Speeds, and $e_{\max} = 10\%$ (Continued)

GUIDE VALUES FOR RAMP DESIGN SPEED (continued)

8-3

CHART 5

US CUSTOMARY

C-5

e (%)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)	R (ft)
	$V_d = 15$ mph $V_d = 20$ mph $V_d = 25$ mph $V_d = 30$ mph $V_d = 35$ mph $V_d = 40$ mph $V_d = 45$ mph $V_d = 50$ mph $V_d = 55$ mph $V_d = 60$ mph $V_d = 65$ mph $V_d = 70$ mph $V_d = 75$ mph $V_d = 80$ mph																	
1.5	950	1890	2860	3370	4390	5580	6910	8370	9990	11800	13200	14800	16400	18100	19700	21300	22900	24500
2.0	700	1250	1820	2490	3280	4140	5130	6220	7430	8740	9840	11000	12300	13600	15000	16400	17800	19200
2.2	631	1130	1620	2250	2850	3750	4640	5640	6730	7930	8920	9980	11000	12100	13200	14300	15400	16500
2.4	574	1030	1500	2060	2690	3420	4240	5150	6150	7240	8160	9160	10200	11200	12300	13400	14500	15600
2.6	526	936	1370	1890	2470	3140	3900	4730	5660	6670	7510	8420	9380	10200	11100	12000	12900	13800
2.8	484	863	1270	1740	2280	2910	3600	4380	5240	6170	6960	7800	8700	9600	10400	11200	12000	12800
3.0	448	799	1170	1620	2120	2700	3350	4070	4840	5740	6480	7270	8110	8910	9710	10500	11300	12100
3.2	417	743	1090	1510	1970	2520	3130	3800	4550	5370	6060	6800	7600	8440	9240	10000	10800	11600
3.4	389	693	1020	1410	1850	2360	2930	3560	4270	5030	5690	6390	7140	7940	8740	9500	10300	11100
3.6	364	649	963	1320	1730	2220	2750	3350	4020	4740	5470	6200	6980	7740	8500	9260	10000	10800
3.8	341	610	896	1250	1630	2090	2600	3180	3790	4470	5160	5860	6590	7300	8000	8700	9400	10100
4.0	321	574	845	1180	1540	1980	2460	2990	3580	4240	4890	5560	6240	6900	7500	8100	8700	9300
4.2	303	542	798	1110	1460	1870	2330	2840	3400	4020	4560	5130	5750	6420	7000	7500	8000	8500
4.4	286	512	756	1050	1390	1780	2210	2700	3240	3830	4340	4890	5490	6120	6700	7200	7700	8200
4.6	271	485	717	997	1320	1690	2110	2570	3080	3650	4140	4670	5240	5850	6400	6900	7400	7900
4.8	257	460	681	948	1260	1610	2010	2450	2940	3480	3960	4470	5020	5610	6120	6600	7100	7600
5.0	243	437	648	904	1200	1540	1920	2340	2810	3330	3790	4280	4810	5380	5900	6400	6900	7400
5.2	231	415	618	862	1140	1470	1840	2240	2700	3190	3630	4110	4620	5170	5670	6170	6670	7170
5.4	220	395	589	824	1090	1410	1760	2150	2590	3060	3490	3950	4440	4980	5480	5980	6480	6980
5.6	209	377	563	788	1050	1350	1690	2080	2480	2940	3360	3800	4280	4800	5260	5700	6100	6500
5.8	199	359	538	754	1000	1300	1620	1960	2380	2830	3230	3660	4130	4630	5060	5460	5860	6260
6.0	190	343	514	723	960	1250	1560	1910	2300	2730	3110	3530	3990	4470	4870	5270	5670	6070
6.2	181	327	492	694	922	1200	1500	1840	2210	2630	3010	3410	3850	4330	4730	5130	5530	5930
6.4	172	312	471	666	886	1150	1440	1770	2140	2540	2900	3300	3730	4190	4600	5000	5400	5800
6.6	164	298	452	639	852	1110	1390	1710	2060	2450	2810	3210	3610	4060	4460	4860	5260	5660
6.8	156	284	433	615	820	1070	1340	1650	1990	2370	2720	3100	3500	3940	4340	4740	5140	5540
7.0	148	271	415	591	790	1030	1300	1590	1930	2290	2630	3000	3400	3820	4220	4620	5020	5420
7.2	140	258	398	568	762	994	1250	1540	1880	2220	2550	2910	3290	3700	4100	4500	4900	5300
7.4	133	246	382	547	734	960	1210	1490	1810	2150	2470	2820	3200	3610	4010	4410	4810	5210
7.6	125	234	366	527	708	928	1170	1440	1750	2090	2400	2740	3120	3520	3920	4320	4720	5120
7.8	118	222	351	507	684	897	1130	1400	1700	2020	2330	2670	3030	3430	3830	4230	4630	5030
8.0	111	210	336	488	660	868	1100	1360	1650	1970	2270	2600	2950	3340	3740	4140	4540	4940
8.2	105	199	321	470	637	840	1070	1320	1600	1910	2210	2530	2880	3270	3670	4070	4470	4870
8.4	100	190	307	452	615	813	1030	1280	1550	1860	2150	2460	2800	3180	3580	3980	4380	4780
8.6	95	180	294	435	594	787	997	1240	1510	1810	2090	2400	2740	3120	3520	3920	4320	4720
8.8	90	172	281	418	574	762	967	1200	1470	1780	2040	2340	2670	3030	3430	3830	4230	4630
9.0	85	164	270	403	554	736	938	1170	1440	1740	2000	2280	2610	2970	3370	3770	4170	4570
9.2	81	156	258	388	535	715	910	1140	1380	1680	1940	2230	2560	2920	3320	3720	4120	4520
9.4	77	149	248	373	516	693	883	1100	1350	1650	1900	2180	2470	2830	3230	3630	4030	4430
9.6	74	142	238	359	499	671	857	1070	1310	1580	1840	2130	2440	2800	3200	3600	4000	4400
9.8	70	136	228	346	481	650	832	1040	1280	1540	1800	2090	2390	2750	3150	3550	3950	4350
10.0	67	130	219	333	465	629	806	1010	1250	1500	1760	2030	2330	2690	3090	3490	3890	4290
10.2	64	124	210	320	448	608	781	980	1210	1460	1720	1990	2240	2540	2840	3140	3440	3740
10.4	61	118	201	308	432	588	757	951	1180	1430	1680	1940	2240	2540	2840	3140	3440	3740
10.6	58	113	192	296	416	568	732	922	1140	1390	1640	1900	2190	2490	2790	3090	3390	3690
10.8	55	108	184	284	400	548	707	892	1110	1360	1610	1870	2160	2460	2760	3060	3360	3660
11.0	52	102	175	272	384	527	682	862	1070	1310	1560	1810	2100	2400	2700	3000	3300	3600
11.2	49	97	167	259	368	506	656	831	1040	1270	1510	1760	2050	2350	2650	2950	3250	3550
11.4	47	92	158	247	351	485	629	799	1000	1220	1470	1710	2000	2300	2600	2900	3200	3500
11.6	44	86	149	233	333	461	600	763	953	1170	1410	1650	1940	2240	2540	2840	3140	3440
11.8	40	80	139	218	312	434	566	722	904	1120	1350	1590	1880	2180	2480	2780	3080	3380
12.0	34	68	119	188	272	381	500	641	807	1000	1220	1480	1790	2130	2470	2810	3150	3490

Exhibit 3-29. Minimum Radii for Design Superelevation Rates, Design Speeds, and $e_{\max} = 12\%$ (Continued)

MAXIMUM RAMP GRADES

8-4

- 1) Desirable ramp grades shall not exceed 5% for a 50 mph design speed, or 6% for a 40 mph design speed, and should not exceed 5% in areas subject to snow and ice.
- 2) Where the ramp is to be used by a high volume of heavy trucks, up grades should be limited to 4%.
- 3) In exceptional cases, as with loops and urban area ramps, grades may be as steep as 10%. However, grades this steep should usually be limited to minor ramps with low volumes. A steep grade on a ramp is not objectionable if the gradient aids acceleration on entrance ramps or deceleration on exit ramps.
- 4) Ramps with high design speeds or those joining high-speed highways generally should have flatter grades than ramps with low design speeds or minor, light-volume ramps.
- 5) Grade should be limited on ramps with sharp horizontal curvature on downgrades as the high rate of superelevation in conjunction with a steep downgrade makes steering difficult.
- 6) If a ramp gradient does not aid the acceleration on entrance ramps or deceleration on exit ramps, care should be taken to provide the appropriate length for speed change.
- 7) Avoid use of Sag Vertical Curves in Cut Sections when possible.

PROCEDURE FOR ESTABLISHING RAMP GRADES WITH CONTROL POINTS

8-5

GIVEN:

- 1) Mainline alignment, stationing, grade, pavement width, and superelevation.
- 2) Ramp alignment, stationing, pavement width, superelevation, and nose station.

FIND: Ramp grade in the area adjacent to the mainline at the exit or entrance point.

PROCEDURE:

- (1) Establish a series of control point elevations along the ramp survey line (or grade point) for the ramp grade to pass thru in order to provide a smooth, driveable pavement surface at the exit or entrance gore.

**PROCEDURE FOR ESTABLISHING RAMP GRADES WITH
CONTROL POINTS (continued)**

8-5

- A) Using a plan sheet with completed horizontal alignment, layout a series of cross-section lines at approximately 25' to 50' intervals at pertinent points along the ramp and mainline alignment. A section should be placed at the beginning station and nose station on the ramp. Sections between these points can be placed at random locations in order to adequately cover the pavement. A section should also be placed 200' to 300' beyond the nose station to check the proposed ditch slopes between the ramp and mainline. See Sketch No. 1 for an example layout.
- B) Using the mainline grade, pavement width, and superelevation, calculate the mainline edge of pavement elevations adjacent to the ramp at those mainline stations selected with the cross-section layout.
- C) Establish a maximum, minimum, and desirable elevation at each ramp station selected with the cross-section layout. The maximum and minimum range is obtained by applying various superelevation rates on the pavement in the "wedge area" between the mainline and ramp edges of pavement. The various rates of superelevation in the "wedge area" are selected by applying a maximum 0.05 "roll-over" at the mainline edge of pavement and then at the ramp edge of pavement adjacent to the wedge area. See Sketch No. 2 for an example. It should be noted that the 0.05 roll-over limit is to be used with discretion in each case so that the resultant superelevation does not create an impractical or awkward section in the wedge area. After selecting a range of superelevation and scaling the width of the "wedge area", calculate the maximum and minimum elevation adjustments, due to the wedge superelevation, at each cross section. An additional superelevation adjustment calculation is made for the area from the ramp edge of pavement to the ramp centerline (4' or 2' width for a single lane ramp). Also a desirable or ideal elevation adjustment is of value in computing the ramp grade. This is calculated by assigning the ideal or most comfortable superelevation in the wedge area. This desirable elevation adjustment will obviously fall within the maximum and minimum range as described above.

At this point, the maximum, minimum, and desirable elevation adjustments are applied to the mainline edge of pavement elevations at each set of stations to provide a series of elevations on the ramp centerline thru which the proposed ramp grade must pass. It is helpful to prepare a chart for listing the various stations and their respective superelevation and elevation adjustments in calculating the maximum, minimum and desirable elevations.

**PROCEDURE FOR ESTABLISHING RAMP GRADES WITH
CONTROL POINTS (continued)**

8-5

- (2) Compute a ramp grade which passes between these calculated elevations.
 - a) Plot a profile with the ramp stationing and the corresponding maximum, minimum and desirable elevation.
 - b) Compute ramp grade with tangents and/or vertical curves to pass thru the desirable elevations with a tolerance of ± 0.04 ft. if possible. If a grade thru the desirable points is not attainable, the maximum- minimum range can be utilized as the limits for the proposed grade. When using the maximum-minimum range, the designer must be careful to avoid using the minimum elevation at a particular station and the maximum elevation at an adjacent station. This situation can result in undesirable random superelevation across the wedge area. When using the maximum-minimum range, the grade should consistently be in the minimum area or in the maximum area to insure uniformity in the wedge area superelevation.
 - c) After the ramp grade is computed thru the gore area, a check of the superelevation "built into" the wedge should be made to insure a uniform pavement.
 - d) After the grade is established in the gore area, it can be continued to the "Y" line with normal grade design procedures.

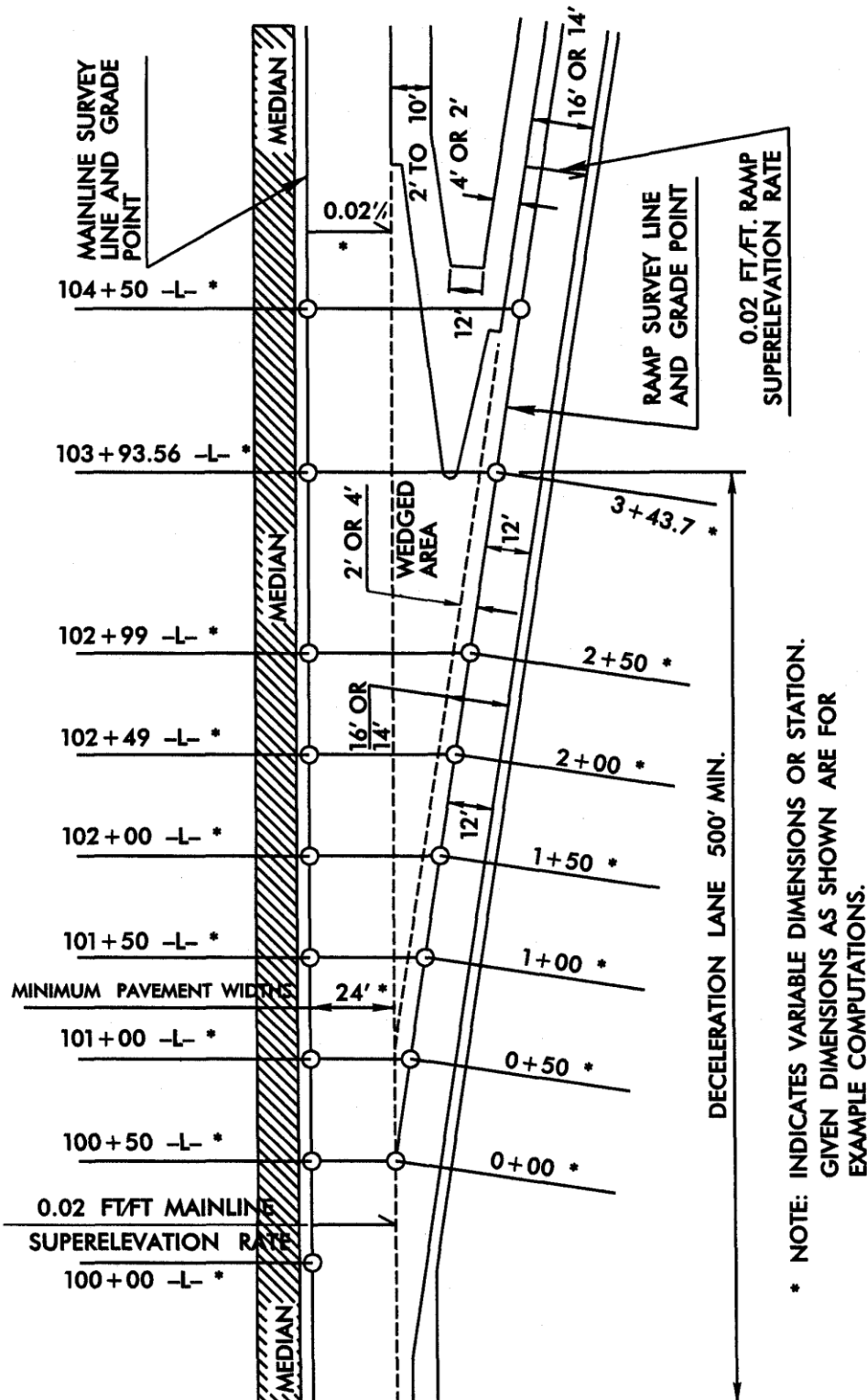
Note: Also see Chapter 8-11 for additional information on the layout of deceleration and acceleration lanes.

See the Roadway Standard Drawings for the Standard Deceleration and Acceleration lanes.

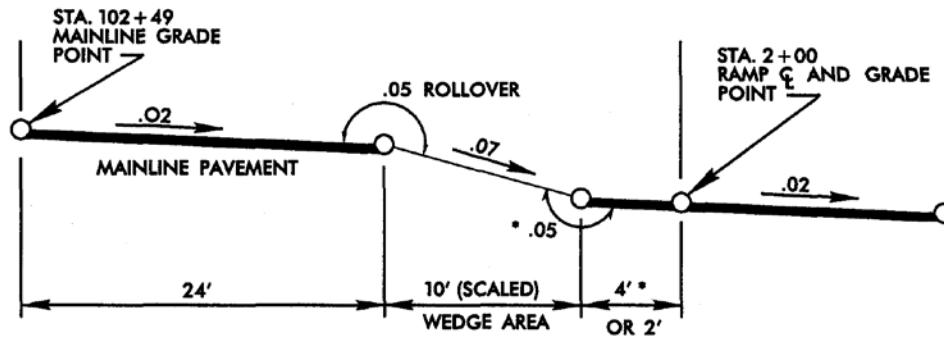
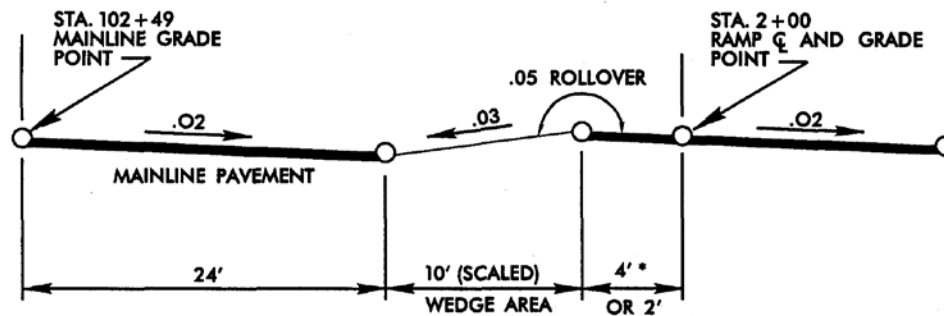
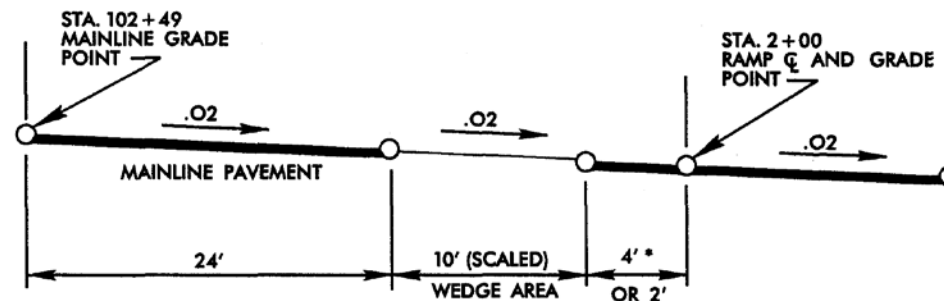
SKETCH 1

8-5

S-1



RAMP GORE GRADE CONTROL POINTS

SKETCH 2**8 - 5****S - 2****MINIMUM ELEVATION DIAGRAM FOR RAMP GRADE AT STATION 2 + 00****MAXIMUM ELEVATION DIAGRAM FOR RAMP GRADE AT STATION 2 + 00****DESIRABLE ELEVATION DIAGRAM FOR RAMP GRADE AT STATION 2 + 00**

NOTE: STATIONS DIMENSIONS AND SUPERELEVATIONS ARE SHOWN AS EXAMPLE SITUATIONS.

* 4' OR 2' DIMENSION DEPENDENT UPON RAMP PAVEMENT WIDTH (16' OR 14')

MAXIMUM/MINIMUM GRADE CONTROL POINTS IN GORE AREA

SIGHT DISTANCE AT DIAMOND RAMP TERMINALS

8-6

See the sight line and geometric measurements. For additional information, see A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (2011), ch. 5. Detail of Measurement of Sight Distance at Ramp Terminals.

With reduced handrail offsets specified in the Bridge Policy (see Chapter 6-1 of this Manual), horizontal sight distance has become a more critical element of interchange design. The more narrow bridge restricts the horizontal sight line, so that now the ramp terminal location, Y-line grade, and handrail offset must be considered in combination to attain the required sight distance across the bridge. Each interchange design must be individually studied to achieve the most cost effective combination of bridge width, ramp terminal location, and Y-line grade. A 6' minimum handrail offset will be used on interchange bridges.

There are four basic options available to the designer for providing the required horizontal sight distances.

1. Design the Y-line grade to enable the driver to see over the bridge handrail and guardrail if present. (Chapter 8-7, Table 1 provides K values for Y-Line grades that will enable the ramp vehicle driver to see over the bridge handrail.)
2. Increase the bridge handrail offset and allow the horizontal sight line to fall inside the handrail. (Chapter 8-7, Table 1 provides K values for Y-Line grades that will allow a clear sight line inside the bridge handrail.)
3. Use the minimum handrail offset required by the Bridge Policy (see Chapter 6-1 of this Manual) and locate the ramp terminal a sufficient distance from the bridge end to provide the required sight distance. (The graph on Chapter 8-7, Table 2 shows the distance required from the end of bridge to ramp terminal that provides required horizontal sight distance with various bridge handrail offset distances. Conversely, this graph can show the available horizontal sight distance with set ramp terminals and handrail offset distances. This graph may also be use to derive combinations of handrail offsets and ramp terminal locations that may be necessary in an economic analysis of the interchange layout.)
4. Consider designing grades with the mainline carried over the Y-line. This design may be cost effective with a narrow median on the mainline and a multilane Y-line. Earthwork costs are usually the critical cost elements in this option.

SIGHT DISTANCE AT DIAMOND RAMP TERMINALS (continued)8-6

Some of the variables that must be considered in the economic evaluation of sight distance design options include grades, horizontal alignment, guardrail, skew, earthwork cost, right of way cost, handrail offset and bridge cost.

Another design element of importance is stopping sight distance from ramps (loops) that exit the mainline from beneath a bridge. The reduced offset from edge of pavement to piers and/or end bent fill slopes may restrict the stopping sight distance in these cases. The proper combination of pier location and ramp alignment should be designed to provide a minimum stopping sight distance of 350 feet.

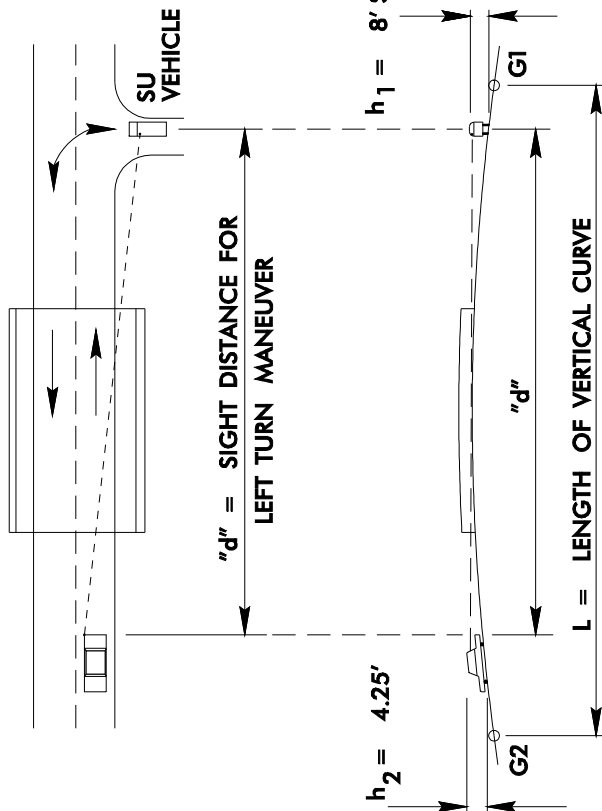
The same attention should be given a ramp (loop) that exits the mainline immediately after crossing a bridge. The proper combination of handrail offset and ramp alignment should be designed so that the handrail does not restrict the required stopping sight distance for the ramp. These sight lines should be checked graphically by the designer.

TABLE 1

CROSSROAD DESIGN SPEED	SIGHT DISTANCE "d" REQ'D. FOR SU RAMP VEHICLE, LEFT TURN MANEUVER ₁	"K" REQ'D. FOR STOPPING SIGHT DISTANCE ALONG CROSSROAD ₂	"K" REQ'D. TO PROVIDE SIGHT DISTANCE "d" FOR SU RAMP VEHICLE LEFT TURN MANEUVER ₃	"K" REQ'D. TO PROVIDE SIGHT DISTANCE "d" FOR SU RAMP VEHICLE SIGHTING OVER BRIDGE RAIL ₄
70 MPH	1060 FT.	247 *	235	442
60 MPH	910 FT.	151 *	173	326
50 MPH	760 FT.	84	121 *	227
40 MPH	610 FT.	44	78 *	147

* DENOTES MINIMUM "K" TO BE USED FOR EACH DESIGN SPEED

VERTICAL SIGHT DISTANCE ELEMENTS



$$K = L/A$$

A = ALGEBRAIC DIFF. IN GRADES (G2 - G1)

VERTICAL SIGHT DISTANCE SHOULD BE PROVIDED IN COMBINATION WITH HORIZONTAL SIGHT CONTROLS. THE DESIGN DATA LISTED ABOVE IS BASED ON UTILIZING THE SU VEHICLE AS THE RAMP VEHICLE. WITH A PASSENGER CAR AS THE RAMP VEHICLE, THE SIGHT DISTANCE PROVIDED WITH THE DESIGN DATA LISTED ABOVE ALLOWS FOR APPROACH SPEEDS GREATER THAN THE CROSSROAD DESIGN. WITH A WB-50, THE AVAILABLE SIGHT DISTANCE ALLOWS FOR APPROACH SPEEDS OF ABOUT 75% OF THE CROSSROAD DESIGN SPEED WHICH IS APPROXIMATELY THE AVERAGE RUNNING SPEED OF THE CROSSROAD TRAFFIC.

NOTES:

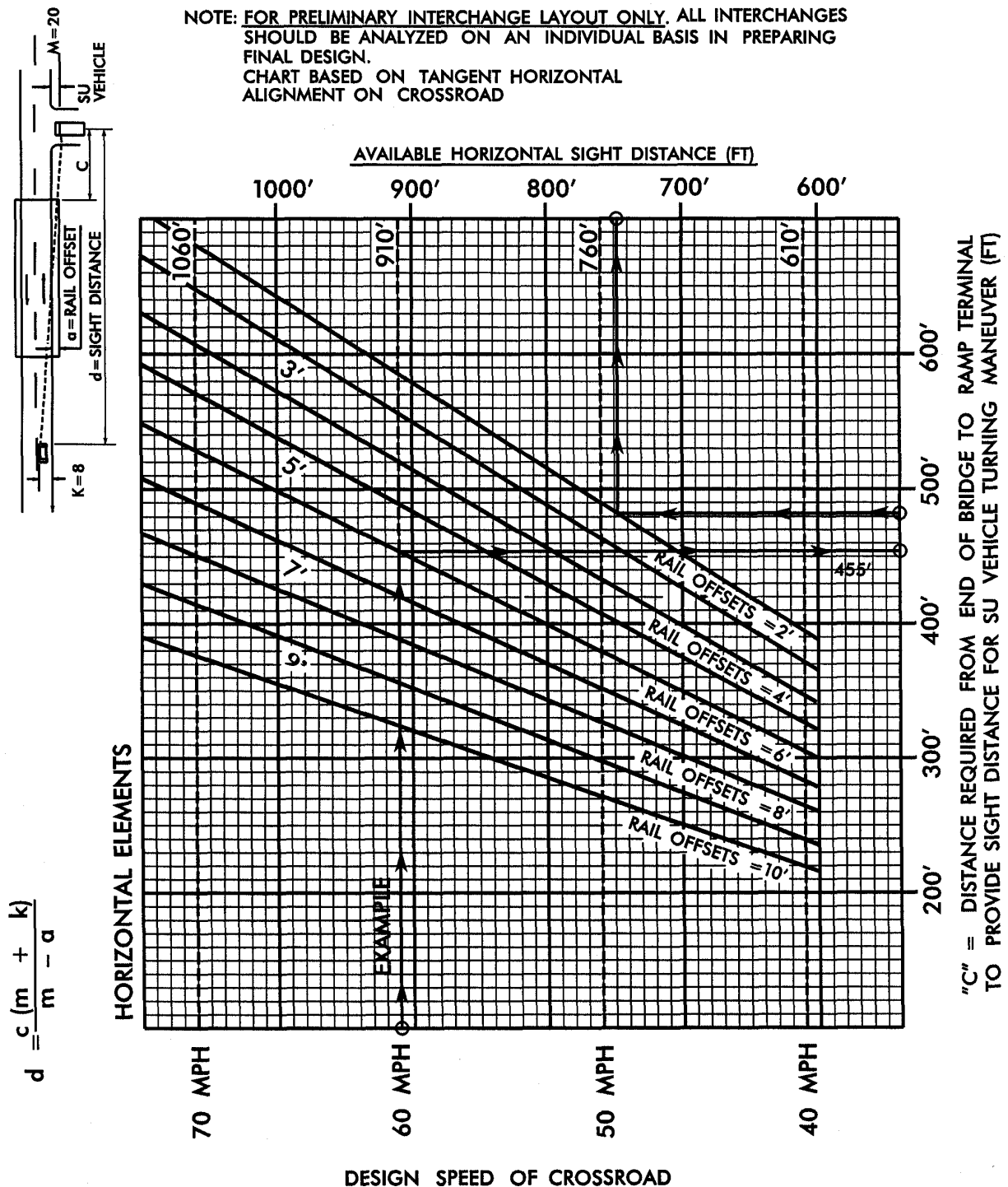
1. SIGHT DISTANCE "d" IS ESTABLISHED BY AASHTO CRITERIA FOR THE SU CONDITION; A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (2004)
2. MINIMUM "K" FOR STOPPING SIGHT DISTANCE ALONG CROSSROAD ACCORDING TO THE 2001 AASHTO CRITERIA
3. DERIVED FROM $K = \frac{d^2}{100 (\sqrt{2h_1} + \sqrt{2h_2})^2}$ WITH $h_1 = 8.0'$, $h_2 = 4.25'$
4. RAMP VEHICLE DRIVER SIGHTS OVER BRIDGE RAIL (2.67' RAIL HT.). RAIL DOES NOT OBSTRUCT HORIZONTAL OR VERTICAL SIGHT LINES FOR REQUIRED "d";
 $h_1 = (8.0' - 2.67') h_2 = (4.25' - 2.67')$

SIGHT DISTANCE OBTAINED BY SIGHTING INSIDE BRIDGE RAIL

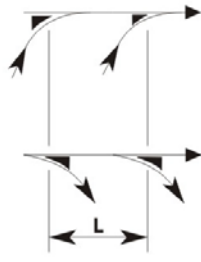
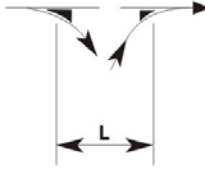
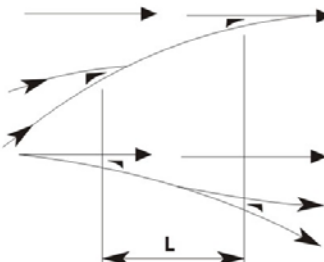
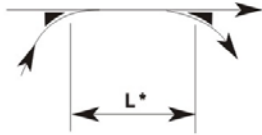
VERTICAL SIGHT DISTANCE CONTROL FOR CREST CURVES
AT DIAMOND INTERCHANGES, SINGLE UNIT VEHICLE CRITERIA

TABLE 2**8 - 7****DESIGN REQUIREMENTS FOR CROSSROAD SIGHT DISTANCE
SINGLE UNIT VEHICLE CRITERIA - DIAMOND INTERCHANGE****T - 2**

NOTE: FOR PRELIMINARY INTERCHANGE LAYOUT ONLY. ALL INTERCHANGES SHOULD BE ANALYZED ON AN INDIVIDUAL BASIS IN PREPARING FINAL DESIGN.
CHART BASED ON TANGENT HORIZONTAL ALIGNMENT ON CROSSROAD



ARRANGEMENT FOR SUCCESSIVE RAMP TERMINALS**8-8****FIGURE 1****8 – 8****RECOMMENDED MINIMUM RAMP TERMINAL SPACING****F - 1**

EN-EN OR EX-EX		EX-EN		TURNING ROADWAYS		EX-EN (WEAVING)			
						 * NOT APPLICABLE TO CLOVERLEAF LOOP RAMPS			
FULL FREEWAY	CDR OR FDR	FULL FREEWAY	CDR OR FDR	SYSTEM INTER- CHANGE	SERVICE INTER- CHANGE	SYSTEM TO SERVICE INTERCHANGE		SYSTEM TO SERVICE INTERCHANGE	
						FULL FWY.	CDR OR FDR	FULL FWY.	CDR OR FDR
MINIMUM LENGTHS MEASURED BETWEEN SUCCESSIVE RAMPS TERMINALS									
1000 ft	800 ft	500 ft	400 ft	800 ft	500 ft	2000 ft	1600 ft	1600 ft	1000 ft

ARRANGEMENT FOR SUCCESSIVE RAMP TERMINALS

NOTES:

FDR – FREEWAY DISTRIBUTOR
CDR – COLLECTOR DISTRIBUTOREN – ENTRANCE
EX – EXIT

THE RECOMMENDATIONS ARE BASED ON OPERATIONAL EXPERIENCE AND NEED FOR FLEXIBILITY AND ADEQUATE SIGNING. THEY SHOULD BE CHECKED IN ACCORDANCE WITH THE PROCEDURE OUTLINED IN THE HIGHWAY CAPACITY MANUAL (4) AND THE LARGER OF THE VALUES IS SUGGESTED FOR USE. ALSO, A PROCEDURE FOR MEASURING THE LENGTH OF THE WEAVING SECTION IS GIVEN IN CHAPTER 24 OF THE 2000 HIGHWAY CAPACITY MANUAL (4) THE "L" DISTANCES NOTED IN THE FIGURES ABOVE ARE BETWEEN LIKE POINTS, NOT NECESSARILY "PHYSICAL" GORES. A MINIMUM DISTANCE OF 270 FT IS RECOMMENDED BETWEEN THE END OF THE TAPER FOR THE FIRST ON RAMP AND THE THEORETICAL GORE FOR THE SUCCEEDING ON RAMP FOR THE EN-EN (SIMILAR FOR EX-EN)

FUTURE GUIDELINES**8-9**

(This section has been reserved for future guidelines.)

MEDIAN DESIGNS IN INTERCHANGE AREAS**8-10**

The median width of a facility should not be reduced through an interchange on either the mainline or the intersecting highway (-Y- Line), if the median is continuous. (See Chapter 1-6 in Part I of this manual.)

Traffic islands on -Y- Lines within the interchange should be provided for highways with four or more lanes. On facilities with three lanes, a 4 foot painted island should be provided. The justification of a left turn lane on the -Y- Line is discussed in 8-15 of this Chapter.

ACCELERATION AND DECELERATION LANES

8-11

Typically on new facilities angular type exit and parallel type entrance ramps should be utilized. When adding or reconstructing an interchange on an existing facility, the designer should maintain the exit and entrance type if a definite pattern has been established on the freeway segment.

Parallel type entrance lanes should be used in locations where existing interchanges facilities are being up-graded and where right of way is at a premium. See Chapter 8-11, Figures 1-2 of this manual for sample deceleration and acceleration lanes. For additional information see Roadway Standard Drawings, Std. No. 225.03.

The designer should provide sufficient length to enable a driver to make the necessary change between the speed of operation on the highway and the speed on the turning roadway in a safe and comfortable manner. The following Figures and Tables show the appropriate method for obtaining the desirable length of a speed change lane, and how the AASHTO values should be applied to the standard entrance and exit types.

CHART 1		MINIMUM ACCELERATION LENGTHS FOR ENTRANCE TERMINALS WITH FLAT GRADES OF TWO PERCENT OR LESS									C-1
US Customary											
Acceleration length, <i>L</i> (ft) for design speed of exit curve <i>V</i> _N (mph)											
Highway design speed, <i>V</i> (mph)	Speed reached, <i>V</i> _{<i>a</i>} (mph)	Stop condition	15	20	25	30	35	40	45	50	
		For average running speed on exit curve, <i>V'</i> _{<i>a</i>} (mph)									
		0	14	18	22	26	30	36	40	44	
30	23	180	140	-	-	-	-	-	-	-	
35	27	280	220	160	-	-	-	-	-	-	
40	31	360	300	270	210	120	-	-	-	-	
45	35	560	490	440	380	280	160	-	-	-	
50	39	720	660	610	550	450	350	130	-	-	
55	43	960	900	810	780	670	550	320	150	-	
60	47	1200	1140	1100	1020	910	800	550	420	180	
65	50	1410	1350	1310	1220	1120	1000	770	600	370	
70	53	1620	1560	1520	1420	1350	1230	1000	820	580	
75	55	1790	1730	1630	1580	1510	1420	1160	1040	780	
<i>V</i>	=	design speed of highway (mph)									
<i>V</i> _{<i>a</i>}	=	average running speed on highway (mph)									
<i>V</i> _N	=	design speed of exit curve (mph)									
<i>V'</i> _{<i>a</i>}	=	average running speed on exit curve (mph)									

NOTE: Uniform 50:1 to 70:1 tapers are recommended where lengths of acceleration lanes exceed 1,300 ft.

REV. DATE : 06/15/11

REVISION 7

ACCELERATION AND DECELERATION LANES (continued)

8-11

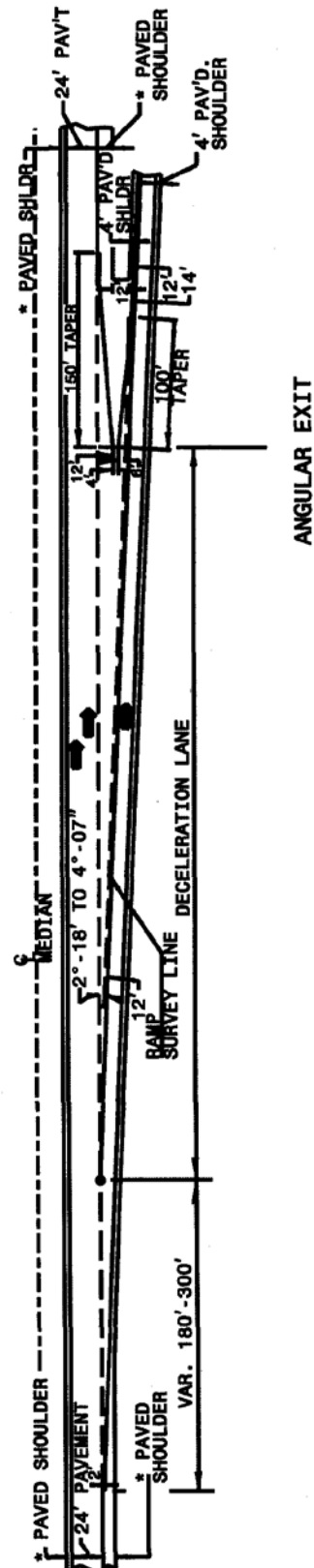
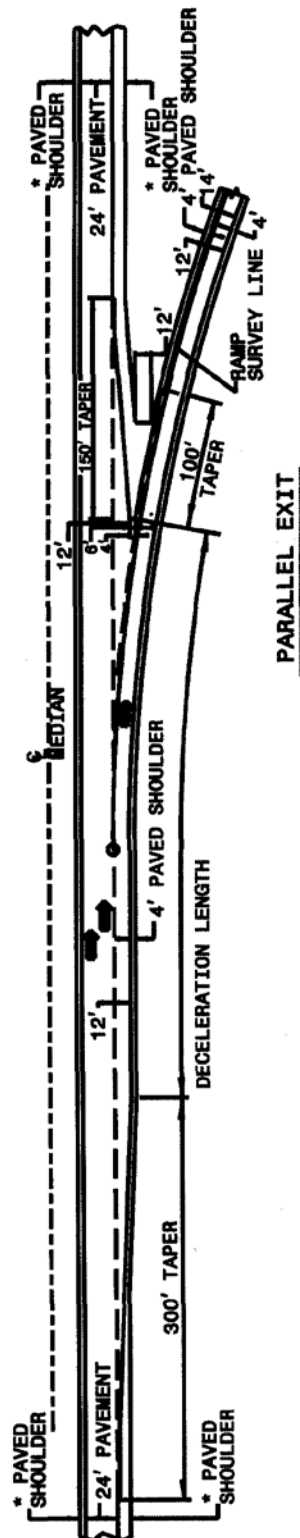
CHART 2		MINIMUM DECELERATION LENGTHS FOR EXIT TERMINALS WITH FLAT GRADES OF TWO PERCENT OR LESS									C-2
US Customary											
Deceleration length, <i>L</i> (ft) for design speed of exit curve <i>V</i> N (mph)											
Highway design speed, <i>V</i> (mph)	Speed reached, <i>V</i> <i>a</i> (mph)	Stop condition	15	20	25	30	35	40	45	50	
		For average running speed on exit curve, <i>V</i> ' <i>a</i> (mph)									
		0	14	18	22	26	30	36	40	44	
30	28	235	200	170	140	—	—	—	—	—	
35	32	280	250	210	185	—	—	—	—	—	
40	36	320	295	265	235	185	155	—	—	—	
45	40	385	350	325	295	250	220	—	—	—	
50	44	435	405	385	355	315	285	225	175	—	
55	48	480	455	440	410	380	350	285	235	—	
60	52	530	500	480	460	430	405	350	300	240	
65	55	570	540	520	500	470	440	390	340	280	
70	58	615	590	570	550	520	490	440	390	340	
75	61	660	635	620	600	575	535	490	440	390	
<i>V</i>	=	design speed of highway (mph)									
<i>V</i> _{<i>a</i>}	=	average running speed on highway (mph)									
<i>V</i> N	=	design speed of exit curve (mph)									
<i>V</i> ' _{<i>a</i>}	=	average running speed on exit curve (mph)									

FIGURE 1

SAMPLE

8-11
F - 1

NOTE: VA=AVERAGE RUNNING SPEED ON HIGHWAY
 V=DESIGN SPEED OF EXIT CURVE (USUALLY
 MEASURED FROM THE SPIRAL TO CURVE
 POINT OF LIMITING CURVE)
 * SEE PAVED SHOULDER POLICY FOR WIDTH.
 PART I CHAPTER 1-40 OF THIS MANUAL



FOR ADDITIONAL INFORMATION, SEE "A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS", EXHIBIT 10-73.

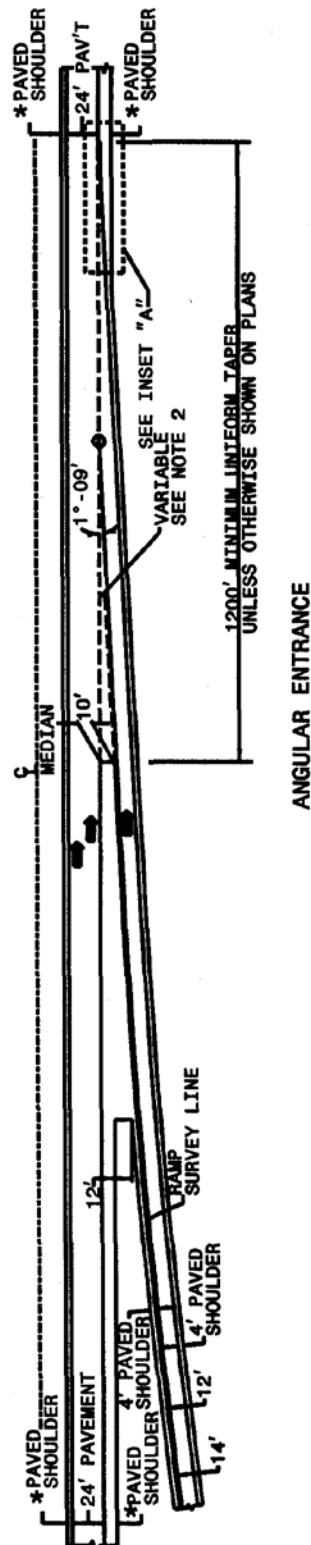
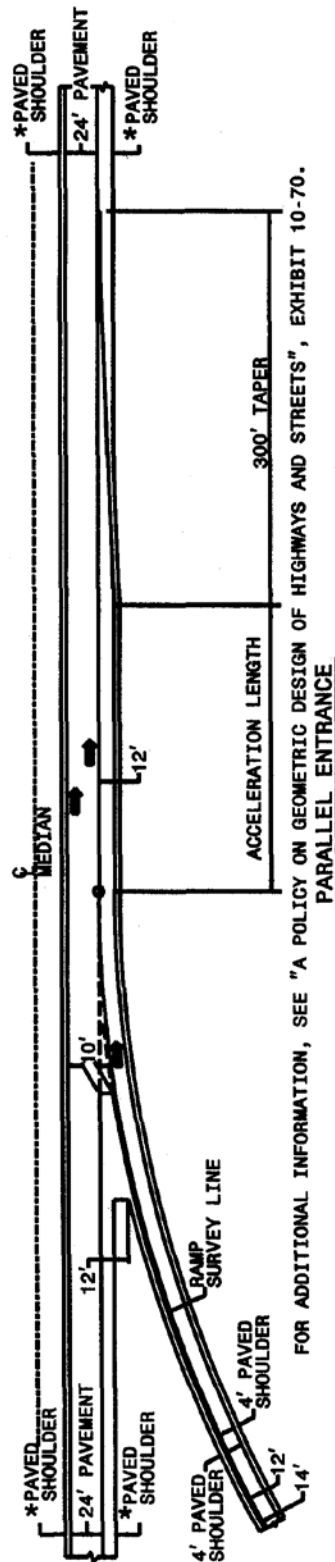
SAMPLE DECELERATION LANE

SAMPLE

FIGURE 2

8 - 11

F - 2



VA=AVERAGE RUNNING SPEED ON HIGHWAY
 V'A=DESIGN SPEED OF ENTRANCE CURVE
 (USUALLY MEASURED FROM THE SPIRAL
 TO CURVE POINT OF LIMITING CURVE)
 * SEE PAVED SHOULDER POLICY FOR WIDTH.
 (PART 1 CHAPTER 1-4 0 OF THIS MANUAL)

SAMPLE ACCELERATION LANE

GRADING AT INTERCHANGES**8-12**

Slopes should be flattened to 4:1 or flatter where feasible within the interchange. This provides better sight distance, eliminates the need for guardrail, and allows for landscaping and mowing.

The designer should provide sight distance on all entrance ramps to allow time for the motorist to adjust their speed to the available gaps in traffic flow. The area beyond the exit gore should provide a traversable safety zone as well as a safe transition to the standard typical section.

For slope transition at bridge endbents, see Roadway Standard Drawings, Std. No's. 225.07 and 225.09.

EARTH BERM MEDIAN PIER PROTECTION**8-13**

See Roadway Standard Drawings, Std. No. 225.08.

RAMP TERMINALS**8-14**

All ramp terminals should be designed to handle the appropriate design vehicle. See Chapter 9 of this manual for additional information.

The designer should pay special attention at ramp terminals to discourage wrong-way entry. At locations with unusual ramp termini configurations, a raised median on the -Y- line may be warranted.

On half-clover type interchanges, the left turning vehicles should be given a recovery area (turning Lane), as shown in Figure 1.

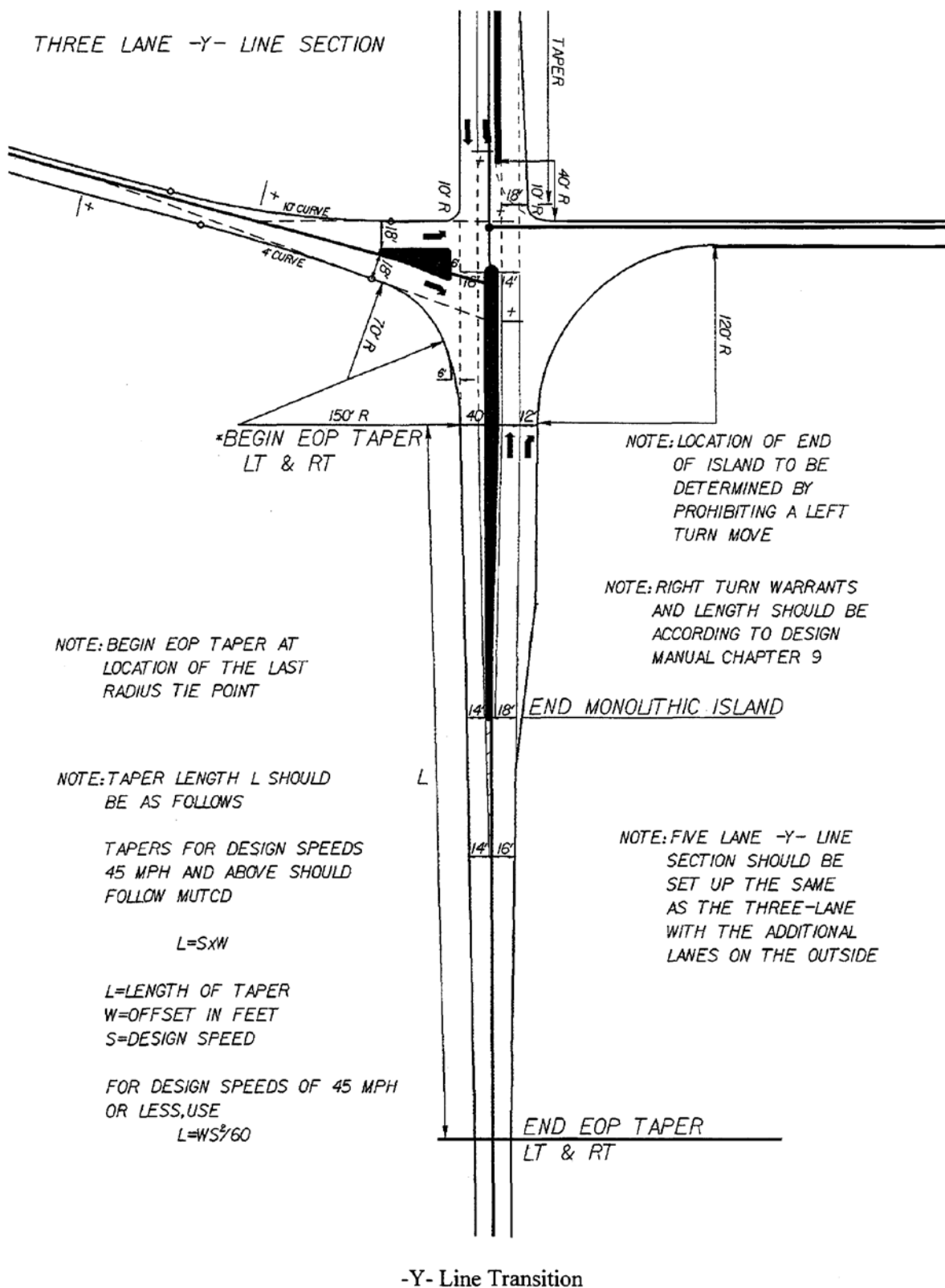
Figure 2 shows designs for ramp terminal radii that will provide safe ingress movements for speeds between 20 and 25 mph. In designing ramps, these designs shall be used as an absolute minimum. Flatter radii may be provided if the designer feels the conditions warrant their use.

-Y- line approach to ramp terminals Figure 3 and 4 show a typical transition for pavement widening at interchange ramp terminals.

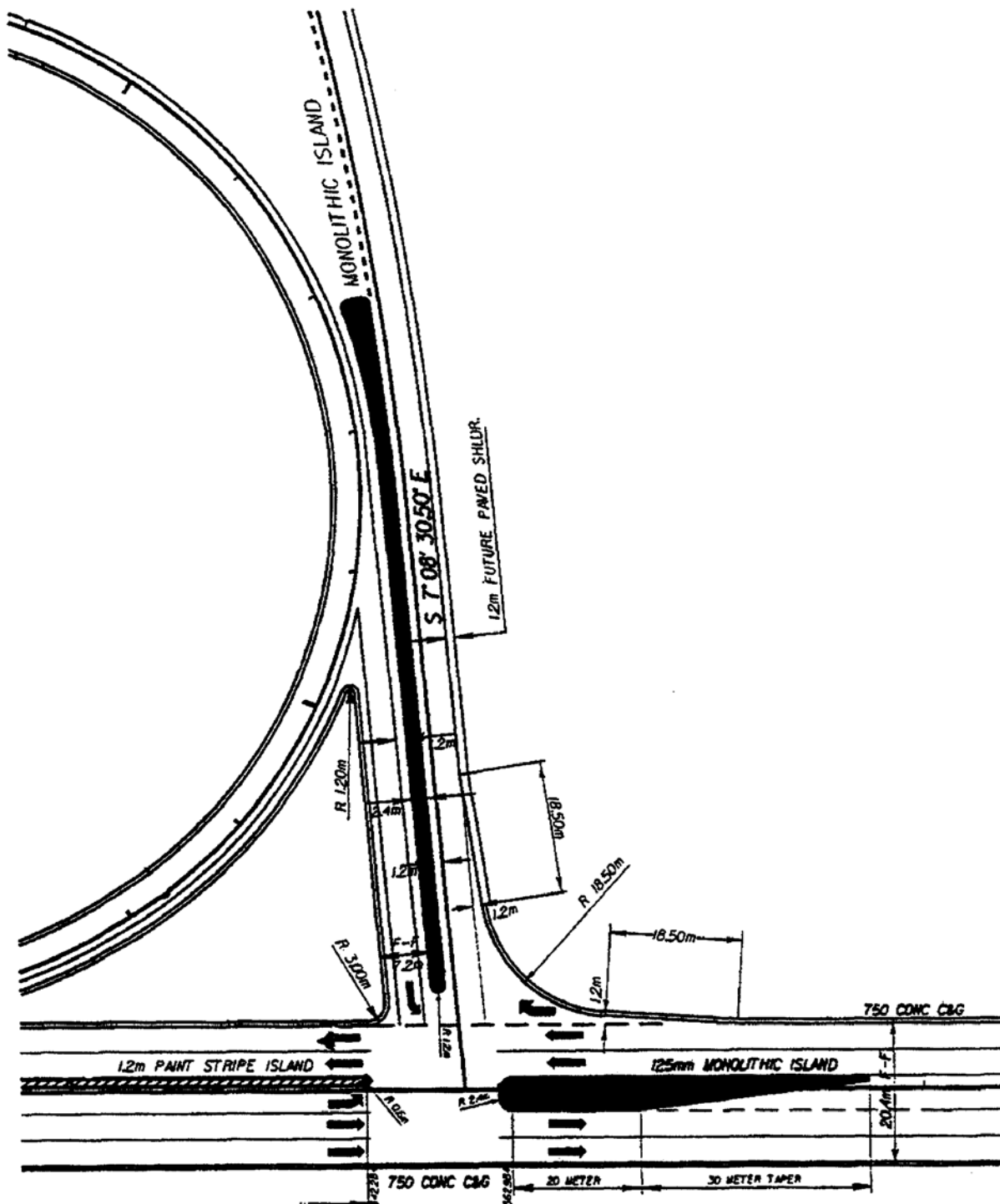
FIGURE 1

8 - 14

F- 1



8 - 14
F - 2



Terminal for Loop Ramp Combination

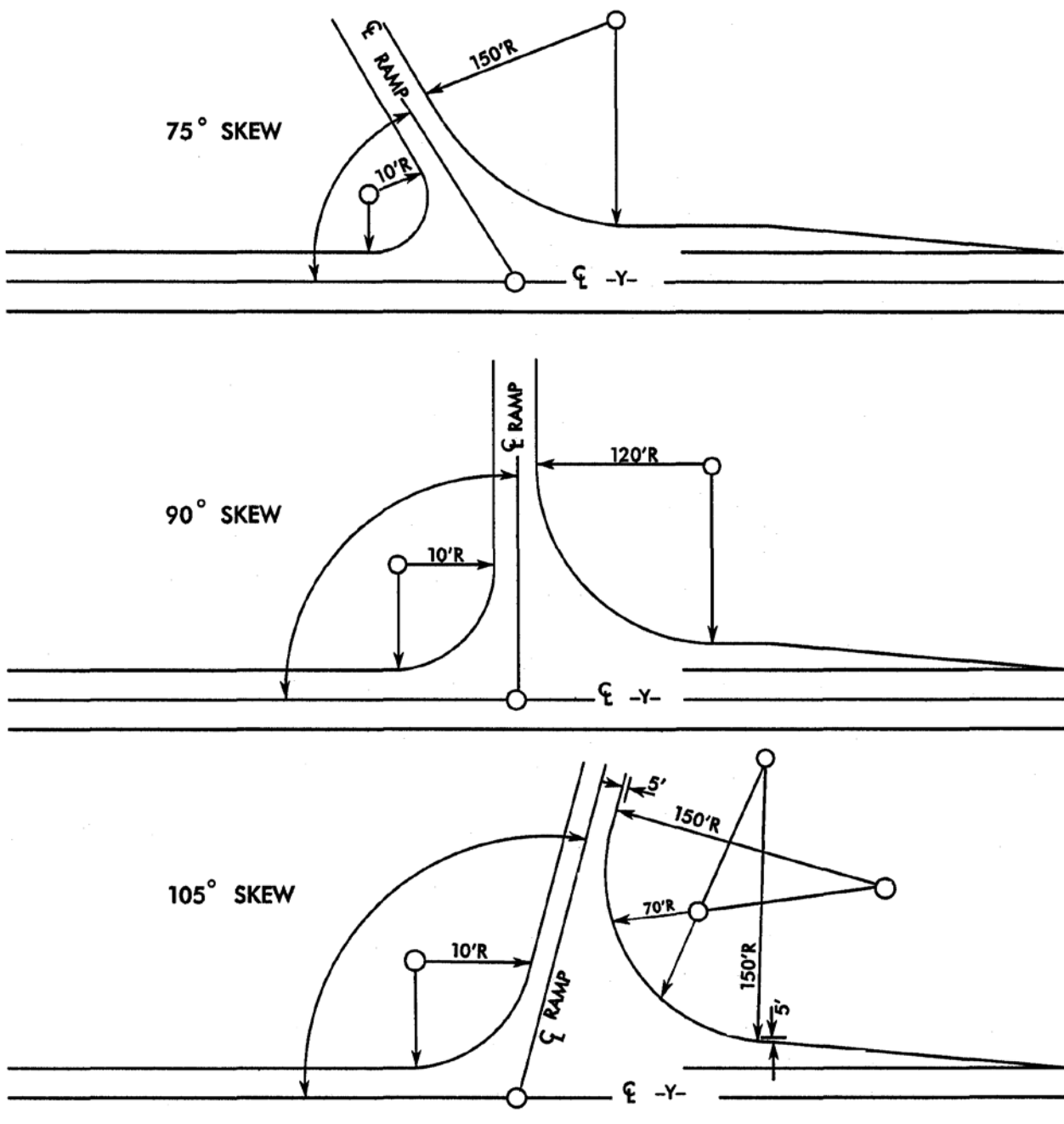
FIGURE 3**8 - 14**
F - 3**SUGGESTED RAMP TERMINAL RADII**

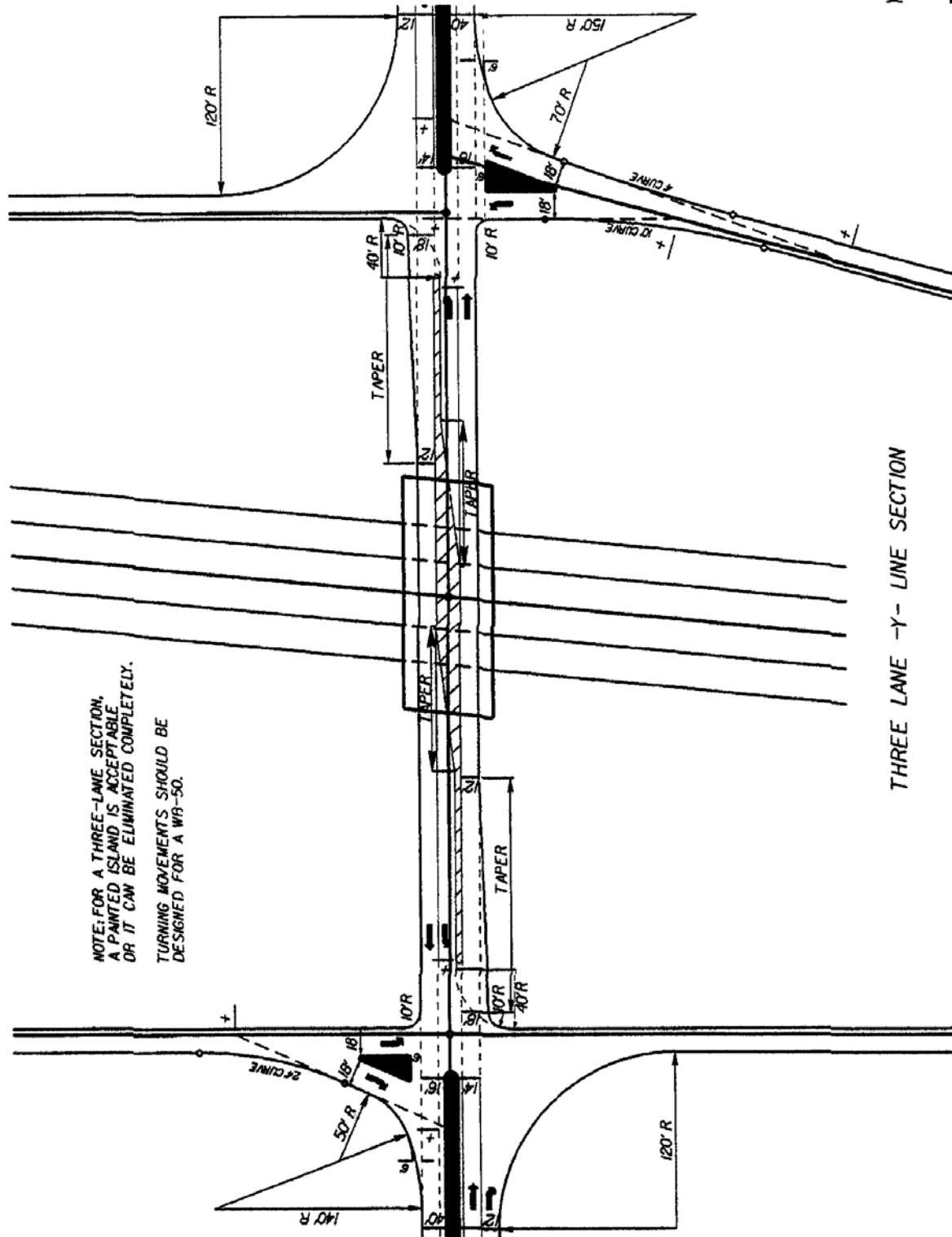
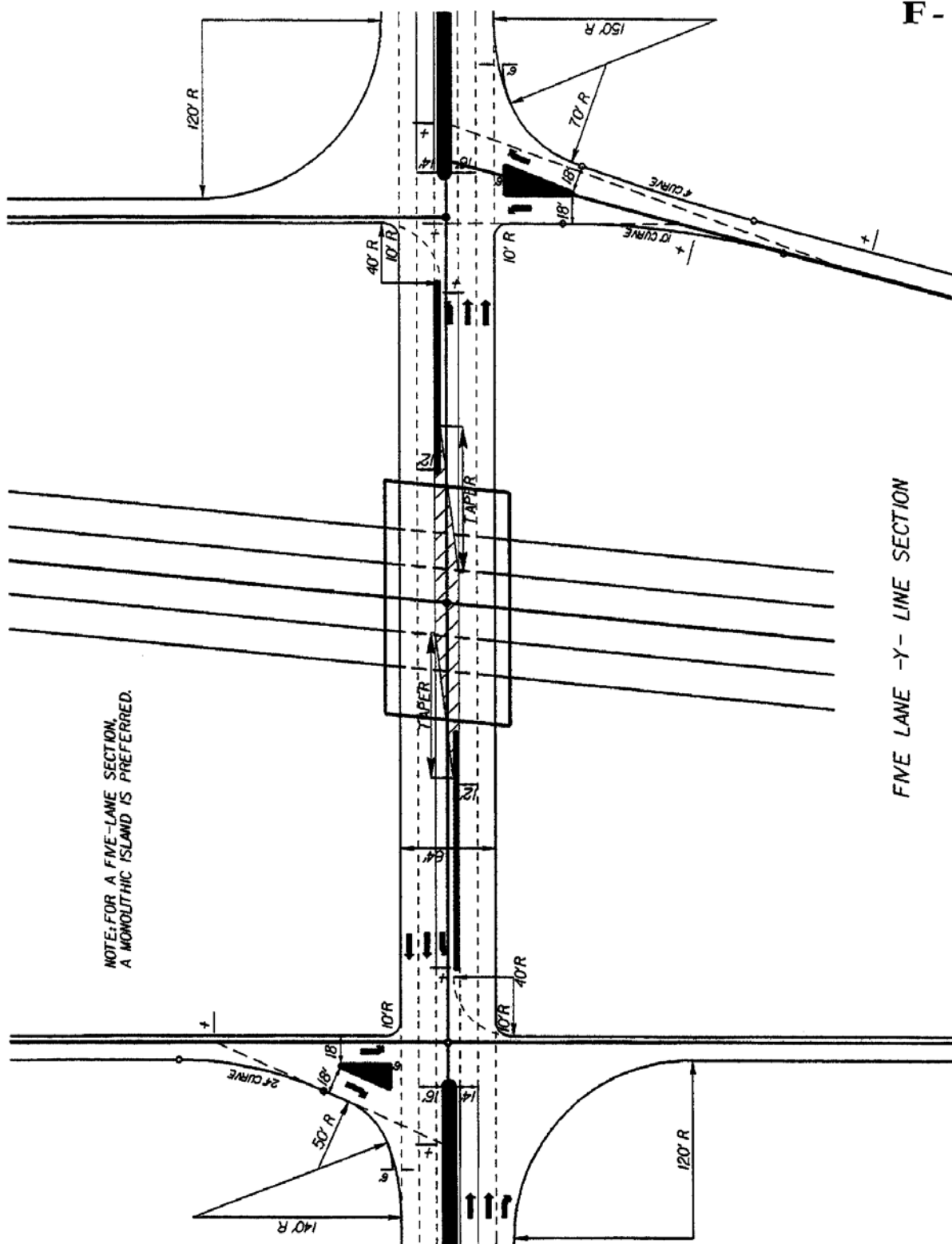
FIGURE 4**8 - 14**
F - 4**RAMP TERMINAL DESIGN**

FIGURE 5

8 - 14
F - 5



RAMP TERMINAL DESIGN

JUSTIFICATION OF LEFT TURN LANES ON TWO-LANE HIGHWAYS

8-15

The need for a left turn lane on an interchange -Y- line should be carefully evaluated by the designer, since it affects the width of the interchange bridge. The need for a left turn lane is determined by traffic volumes, speed, and safety benefits.

The method for determining the warrants for left turn lanes at unsignalized at-grade intersections (applicable to interchange ramp terminals) is addressed in the attached nomograph. The method utilizes a nomograph based on opposing volumes, left turn volumes, and through volumes. The time delays and queuing characteristics of the traffic volumes are the criteria utilized in establishing these nomographs.

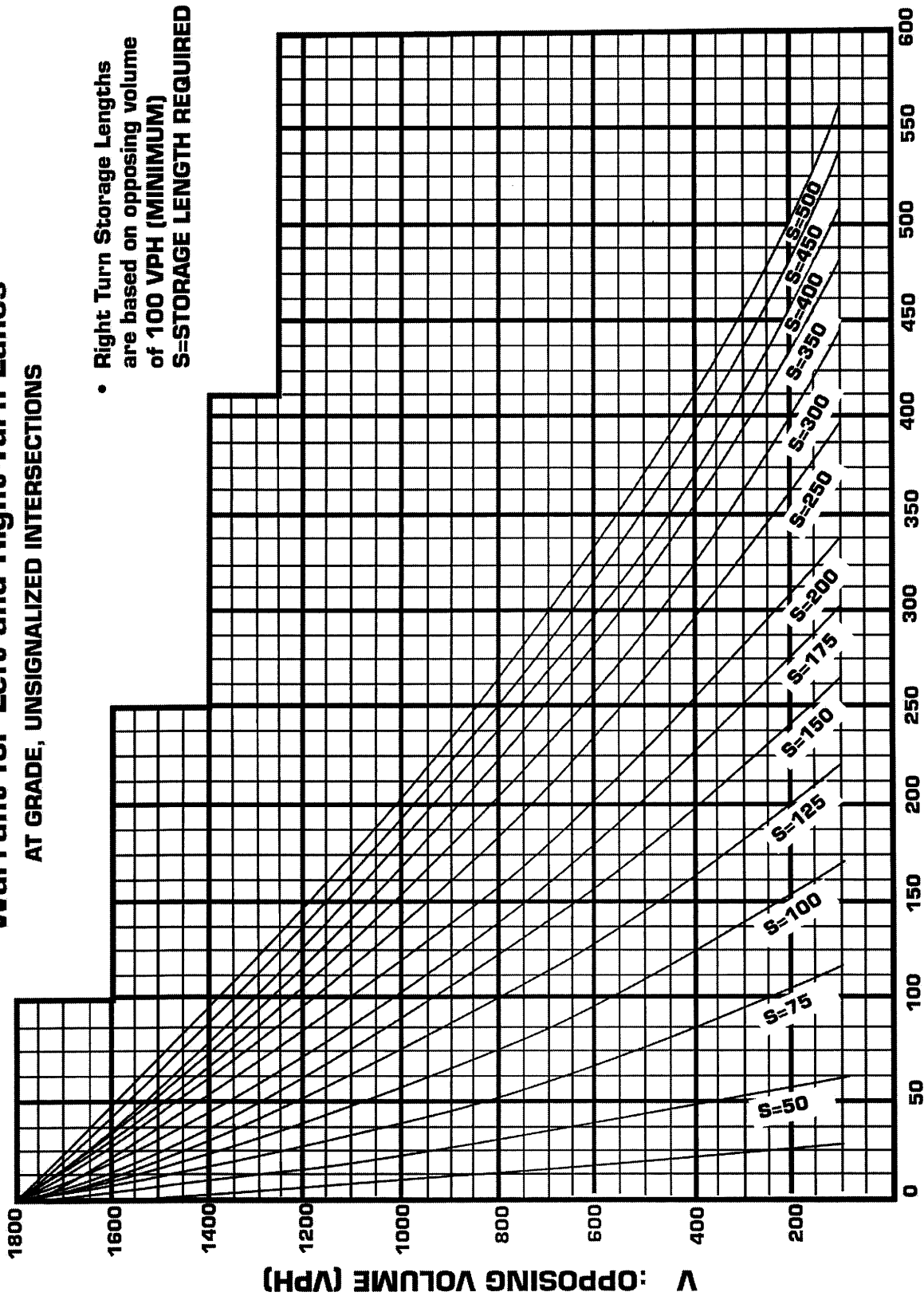
The elements to be used in entering the appropriate nomograph are:

- Operating speed (see A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (2011), ch. 2).
- V_o , opposing traffic volume
- V_L , left turning volume(VPH)
- V_a , advancing traffic volume, including through, left turning, and right turning vehicles (design hour volume).
- V_R , right turning volume(VPH)
- S , storage length required

If the intercept of V and V_a falls right of the applicable S line, that is the amount of storage warranted.

Warrant for Left and Right-Turn Lanes AT GRADE, UNSIGNALIZED INTERSECTIONS

- Right Turn Storage Lengths are based on opposing volume of 100 VPH (MINIMUM)
S=STORAGE LENGTH REQUIRED



Note: Where adjacent signalization may provide opportunities for gaps in the traffic stream a reduction in the above storage values can be considered on a case by case basis.

V_L: LEFT TURNING VOLUME (VPH)
V_R: RIGHT TURNING VOLUME (VPH)