# Procedure for Identification and Investigation of Horizontal Curves with Insufficient Superelevation Rates

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#### **EXECUTIVE SUMMARY**

NCDOT has the second largest highway mileage of any state in the nation. Many of these roads were constructed using older design standards for horizontal curves and superelevation that may not be suitable for current operating speeds and design standards. This is especially relevant for older two-lane, two-way highways, where perhaps hundreds of horizontal curves in each county may be affected by these new standards. A method is needed that can help NCDOT field engineers quickly and reliably evaluate the existing superelevation rate and radius for any curve against current AASHTO design standards which are adopted in the NCDOT Roadway Design Manual. Having a quick and reliable method will enable NCDOT to rapidly investigate any horizontal curve against current design standards and make recommendations for corrective action, if needed.

Of special concern is the change over time in the design standards as recommended by AASHTO in their book "A Policy on Geometric Design of Highways and Streets," commonly referred to as the Green Book. These changing standards mean that previous designs may not meet current standards. One application of this is for horizontal curves, where the superelevation may not be enough for the intended speed of the vehicle. Another application is along the curve itself for safe stopping sight distance (SSD). Both of these issues impact the safety of the traveling public. There may be hundreds of substandard curves in each county that could be improved to meet current standards.

A simple procedure was developed that can take several field measurements, including the superelevation rate, and convert them into the radius of the curve. These values can then be compared to design standards that are presented in charts for direct review in the field without the need for calculations or coming back to the office. If a curve is found to be deficient, then the engineer can look at possible corrective action while on-site. This will be an extremely efficient field investigation of horizontal curves against current design standards. Another aspect of the investigation is a quick method to estimate whether or not SSD is provided through the curve.



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#### INTRODUCTION

NCDOT has the second largest highway mileage of any state in the nation. Many of these roads were constructed using older design standards for horizontal curves and superelevation that may not be suitable for current operating speeds and design standards. This is especially relevant for older two-lane, two-way highways, where perhaps hundreds of horizontal curves in each county may be affected by these new standards. A method is needed that can help NCDOT field engineers quickly and reliably evaluate the existing superelevation rate and radius for any curve against current American Association of State Highway and Transportation Officials (AASHTO) design standards which are adopted in the NCDOT Roadway Design Manual. Having a quick and reliable method will enable NCDOT to rapidly investigate any horizontal curve against current design standards and make recommendations for corrective action, if needed.

Of special concern is the change over time in the design standards as recommended by AASHTO in their book "A Policy on Geometric Design of Highways and Streets," commonly referred to as the Green Book. These changing standards mean that previous designs may not meet current standards. One application of this is for horizontal curves, where the superelevation may not be enough for the intended speed of the vehicle. Another application is along the curve itself for safe stopping sight distance (SSD). Both of these issues impact the safety of the traveling public. There may be hundreds of substandard curves in each county that could be improved to meet current standards.

A simple procedure was developed that can take several field measurements, including the superelevation rate, and convert them into the radius of the curve. The radius and measured values can then be compared to design standards through a set of charts for direct review in the field without the need for calculations or coming back to the office. If a curve is found to be deficient, then the engineer can look at possible corrective action while on-site. This will be an extremely efficient field investigation of horizontal curves against current design standards. Another aspect of the investigation is a quick method to estimate whether or not SSD is provided through the curve.



#### LITERATURE REVIEW

#### INTRODUCTION

The Chord Method can help NCDOT field engineers quickly and reliably evaluate the existing superelevation rate and radius for any curve against current AASHTO design standards. Documentation of literature findings on the best practices for crash reconstruction practices will also help in future investigations by NCDOT. AASHTO design superelevation criteria for maximum superelevation, design superelevation, design speed, and minimum radius were also examined.

#### STATE OF THE PRACTICE

Curve Investigation Techniques

An investigation in Texas compared the accuracy of ten curve radius estimating procedures (Carlson, Burris, Black, & Rose, 2005). The research compared each of the methods to the field survey which found that none of the methods were statistically inaccurate. The methods examined included:

- Basic ball bank indicator (BBI)
- Advanced BBI
- Chord length
- Compass
- Field survey
- Global Positioning System (GPS) unit
- Lateral acceleration
- Plan sheet
- Speed advisory plate
- Vehicle yaw rate

The advanced BBI and vehicle yaw rate methods were not examined past the initial stages of research. The GPS, plan sheet, and chord length methods had the smallest average relative errors of less than  $\pm 5\%$ . A cost analysis was conducted for each of the



techniques that were examined in detail (Exhibit 1). The plan sheet, speed advisory plate, compass, and chord length methods were each under \$150 for the initial cost.

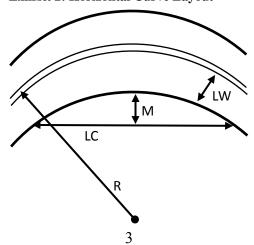
Exhibit 1: Radius Method Cost Analysis (Adapted from Carlson, et al 2005)

| Mathad               | Initial   | Cost Per Curve (\$) |            |  |
|----------------------|-----------|---------------------|------------|--|
| Method               | Cost (\$) | 10 Curves           | 100 Curves |  |
| Basic BBI            | \$560     | \$101               | \$51       |  |
| Chord length         | \$145     | \$75                | \$62       |  |
| Compass              | \$130     | \$28                | \$16       |  |
| Field survey         | \$11,000  | \$1,220             | \$230      |  |
| GPS unit             | \$530     | \$57                | \$9        |  |
| Lateral acceleration | \$5,600   | \$605               | \$101      |  |
| Plan sheet           | \$0       | \$38                | \$38       |  |
| Speed advisory plate | \$15      | \$9                 | \$8        |  |

#### Chord Method of Radius Estimation

The Chord Method is a method that allows a single investigator to determine the radius of a horizontal curve. The Chord Method functions as a viable one-person field investigation method by eliminating the need for determining the deflection angle, delta  $(\Delta)$ , of the horizontal curve. A survey crew is typically required to accurately determine delta, but a single person can execute the Chord Method. A chord (C, or LC) of known length should be placed between two points along the edge of the edge-line of the roadway. Each end of the chord must be within the limits of the curve (between the point of curvature and point of tangency of a single radius horizontal curve). At the mid-point of the chord, a measurement of the middle ordinate (M) should be taken from the chord to the edge of the edge-line. The lane width (LW) should also be measured at the time of the field investigation (Exhibit 2).

**Exhibit 2: Horizontal Curve Layout** 





In order to determine the horizontal curve radius (R) without knowing the deflection angle ( $\Delta$ ), the following derivation and resulting equation can be utilized.

Starting with standard horizontal curve equations for Middle Ordinate (M) and Long Chord (LC):

$$M = R_{EL} \left( 1 - \cos \frac{\Delta}{2} \right)$$
 or  $\frac{M}{R_{EL}} = 1 - \cos \frac{\Delta}{2}$ 

$$LC = 2R_{EL} \sin \frac{\Delta}{2}$$
 or  $\frac{LC}{2R_{EL}} = \sin \frac{\Delta}{2}$ 

Now, 
$$\frac{M}{R_{EL}} = 1 - \cos \frac{\Delta}{2} \qquad \text{or} \qquad -1 + \frac{M}{R_{EL}} = -\cos \frac{\Delta}{2}$$

Multiply by -1: 
$$1 - \frac{M}{R_{EL}} = \cos \frac{\Delta}{2}$$

Square Equation: 
$$\left(1 - \frac{M}{R_{EL}}\right)^2 = \left(\cos\frac{\Delta}{2}\right)^2$$

Also: 
$$\left(\frac{LC}{2R_{FL}}\right)^2 = \left(\sin\frac{\Delta}{2}\right)^2$$

Recall: 
$$(\sin \Delta)^2 + (\cos \Delta)^2 = 1$$
  $\left[ \Delta \operatorname{can be} \frac{\Delta}{2} \operatorname{as well} \right]$ 

Thus: 
$$\left(1 - \frac{M}{R_{EL}}\right)^2 + \left(\frac{LC}{2R_{EL}}\right)^2 = \left(\cos\frac{\Delta}{2}\right)^2 + \left(\sin\frac{\Delta}{2}\right)^2 = 1$$

Expand: 
$$1 - \frac{2M}{R_{EL}} + \frac{M^2}{{R_{EL}}^2} + \frac{LC^2}{4{R_{EL}}^2} = 1$$

Simplify: 
$$-\frac{2M}{R_{EL}} + \frac{M^2}{R_{EL}^2} + \frac{LC^2}{4R_{EL}^2} = 0$$

Multiply by R<sup>2</sup>: 
$$-2M R_{EL} + M^2 + \frac{LC^2}{4} = 0$$

Solve for R<sub>EL</sub>: 
$$R_{EL} = \frac{M^2 + 0.25LC^2}{2M}$$

Therefore: 
$$R = R_{FL} + LW$$



Final Equation (multiply by 4): 
$$R = \frac{4M^2 + C^2}{8M} + LW$$

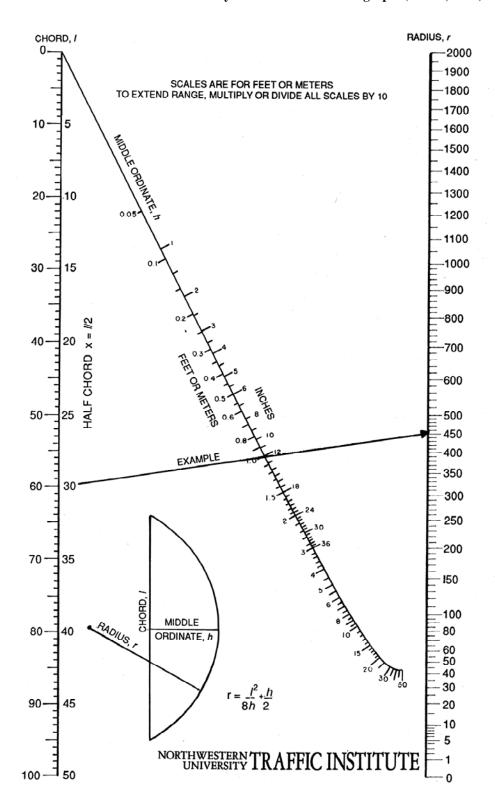
Note that the long chord (LC) has been substituted with any chord length (C) in the final equation.

The final equation for determining the radius (R) of the centerline of the roadway is to add the lane width of the roadway to the radius of the edge-line, where C is a chord of known length, M is the middle ordinate distance measured at the midpoint of the chord, and LW is the measured lane width of the inside lane. The preceding derivation and equation are consistent with commonly accepted field procedures for establishing the radius of horizontal curves (Fricke, 1990; Carlson, Burris, Black, & Rose, 2005).

A nomograph developed by Northwestern University's Traffic Institute provides the ability for dynamic chord lengths (Fricke, 1990). The nomograph allows the user to use any chord length and its corresponding middle ordinate distance to determine the radius of the curve under investigation (Exhibit 3).



Exhibit 3: Northwestern University Traffic Institute Nomograph (Fricke, 1990)





#### AASHTO Green Book

One especially significant reason for doing this project is the recent change in the 2004 AASHTO Green Book on relating the minimum horizontal radius to the superelevation and coefficient of side friction (f) for a given design speed. The 2004 values for 'f' are much different at speeds  $\leq$  45 mph (AASHTO, 2004).

**Exhibit 4: AASHTO Limiting Values of Coefficient of Side Friction** 

|              | Exhibit 4: Migiti o Emitting values of coefficient of side i frection |                        |  |  |  |  |  |
|--------------|---|------------------------|--|--|--|--|--|
| Design Speed | 2001 AASHTO   | 2004 AASHTO            |  |  |  |  |  |
| (mph)        | Limiting Values of 'f'  | Limiting Values of 'f' |  |  |  |  |  |
| 10           |   | 0.38                   |  |  |  |  |  |
| 15           | 0.175   | 0.32                   |  |  |  |  |  |
| 20           | 0.170   | 0.27                   |  |  |  |  |  |
| 25           | 0.165   | 0.23                   |  |  |  |  |  |
| 30           | 0.16  | 0.20                   |  |  |  |  |  |
| 35           | 0.155   | 0.18                   |  |  |  |  |  |
| 40           | 0.150   | 0.16                   |  |  |  |  |  |
| 45           | 0.145   | 0.15                   |  |  |  |  |  |
| 50           | 0.140   | 0.14                   |  |  |  |  |  |
| 55           | 0.130   | 0.13                   |  |  |  |  |  |
| 60           | 0.120   | 0.12                   |  |  |  |  |  |
| 65           | 0.110   | 0.11                   |  |  |  |  |  |
| 70           | 0.100   | 0.10                   |  |  |  |  |  |
| 75           | 0.090   | 0.09                   |  |  |  |  |  |
| 80           | 0.080   | 0.08                   |  |  |  |  |  |

Now, with the new side friction values, the 2004 Green Book calculates the minimum radius to the nearest foot, without rounding up like the 2001 Green Book, as shown in Exhibit 5 for an 8.0% superelevation value.



Exhibit 5: AASHTO Minimum Radius (e<sub>max</sub> 8%)

|              | o william rada |             |             |
|--------------|----------------|-------------|-------------|
| Design Speed | Maximum e      | 2001 AASHTO | 2004 AASHTO |
| (mph)        | (%)            | Minimum R   | Minimum R   |
| 10           | 8.0            |             | 14          |
| 15           | 8.0            | 60          | 38          |
| 20           | 8.0            | 105         | 76          |
| 25           | 8.0            | 170         | 134         |
| 30           | 8.0            | 250         | 214         |
| 35           | 8.0            | 350         | 314         |
| 40           | 8.0            | 465         | 444         |
| 45           | 8.0            | 600         | 587         |
| 50           | 8.0            | 760         | 758         |
| 55           | 8.0            | 965         | 960         |
| 60           | 8.0            | 1205        | 1200        |
| 65           | 8.0            | 1485        | 1480        |
| 70           | 8.0            | 1820        | 1810        |
| 75           | 8.0            | 2215        | 2210        |
| 80           | 8.0            | 2675        | 2670        |

Granted, these are minor differences, especially above 45 mph, but they do impact horizontal curve design. These values for minimum radius are a balance between the maximum superelevation and radius for a given design speed. If the radius is larger than the minimum, then the superelevation rate can be lowered to provide a new balance of the forces on the vehicle as it goes through the curve. The 2004 AASHTO Green Book uses a different approach than the 2001 version to correlate superelevation to radius. The 2004 version provides superelevation (e) on the left column and then the specific radius that matches that e for each design speed. The 2001 version provides a rounded radius on the left column and then shows the matching e needed for each design speed. And in both the 1965 and 1973 versions, degree of curve is on the left column with matching superelevation rates under each design speed. An example of the differences between these versions is shown in Exhibit 6 for 8% superelevation and 60 mph design speed.



| <b>Exhibit 6: AASHTO Radius Differences</b> | $(e_{-} = 8\%)$                                | Design St | need = 60 mnh  |
|---|--|-----------|----------------|
| Exhibit 0. Middli 0 Radius Differences      | $(\mathbf{c}_{\mathbf{max}} - \mathbf{o}_{i})$ | DUSIEND   | occu — oo mpn, |

|                | tadias Bilierences (e <sub>max</sub> – | 070, Besign Speed - | · · · · · · · · · · · · · · · · · · · |
|----------------|--|---------------------|---------------------------------------|
| Superelevation | 1965 & 1973                            | 2001 Radius         | 2004 Radius                           |
| (%)            | Radius (ft)                            | (ft)                | (ft)                                  |
| NC             | 22,918                                 | 23,000 – 12,000     | n/a                                   |
| 2.0            | 11,459                                 | 10,000              | 8,440                                 |
| 2.1            | 9,549 *                                | 8,000               | 8,030 *                               |
| 2.7            | 6,275 *                                | 6,000               | 6,100 *                               |
| 3.2            | 5,210 *                                | 5,000               | 5,040                                 |
| 3.9            | 3,995 *                                | 4,000               | 4,015 *                               |
| 4.4            | 3,475 *                                | 3,500               | 3,470                                 |
| 5.0            | 2,950 *                                | 3,000               | 2,960                                 |
| 5.7            | 2,485 *                                | 2,500               | 2,490 *                               |
| 6.6            | 1,965 *                                | 2,000               | 2,010                                 |
| 7.1            | 1,730 *                                | 1,800               | 1,770 *                               |
| 7.5            | 1,535 *                                | 1,600               | 1,580 *                               |
| 7.8            | 1,340 *                                | 1,400               | 1,410                                 |
| 8.0            | 1,146                                  | 1,205               | 1,200                                 |

<sup>\*</sup> Interpolated value

Again, these radii are close to each other, but not an exact match. Clearly there is judgment being left to the engineer on exactly what to use in each situation if there is not a perfect match between radius and e for a specific curve layout.

Another aspect of the problem is the recent change in the 2001 AASHTO Green Book for stopping sight distance (SSD) calculation. This formula has changed and a new rate of deceleration is applied. The new formula is:  $SSD = 1.47Vt + 1.075\frac{V^{11}}{C}$ 

Thus, new SSD values are calculated for each design speed as shown in Exhibit 7.



**Exhibit 7: AASHTO Stopping Sight Distance Differences** 

| Design Speed | 1965 AASHTO     | 1973 AASHTO     | 1984 AASHTO     | 2001 AASHTO     |
|--------------|-----------------|-----------------|-----------------|-----------------|
| (mph)        | Min. Design SSD | Min. Design SSD | Min. Design SSD | Min. Design SSD |
| (mpn)        | (ft)            | (ft)            | (ft)            | (ft)            |
| 15           |                 |                 |                 | 80              |
| 20           |                 |                 | 125             | 115             |
| 25           |                 |                 | 150             | 155             |
| 30           | 200             | 200             | 200             | 200             |
| 35           |                 |                 | 250             | 250             |
| 40           | 275             | 275             | 325             | 305             |
| 45           |                 |                 | 400             | 360             |
| 50           | 350             | 350             | 475             | 425             |
| 55           |                 |                 | 550             | 495             |
| 60           | 475             | 475             | 650             | 570             |
| 65           | 550             | 550             | 725             | 645             |
| 70           | 600             | 600             | 850             | 730             |
| 75           | 675             |                 |                 | 820             |
| 80           | 750             |                 |                 | 910             |

As can be seen, differences in SSD occur for all but two design speeds, 30 and 35 mph, between the 1984 and 2001 Green Books. Most of the highways where there may be problems with superelevation would be on highways with posted speed limits greater than 40 mph. These values are also different for many design speeds based on earlier versions of the AASHTO Green Book (red cover in 1973 and blue cover in 1965).

These new SSD values are then entered into formulas for determining the minimum length of vertical curve needed to satisfy SSD criteria and can be correlated to the appropriate horizontal curve radius that satisfies SSD criteria as well.

Design inconsistencies in the AASHTO Green Book have been identified in previous research. The selection of different maximum superelevation rates in the Green Book affects superelevation rate although the actual design speed and radius are identical. A superelevation distribution method that accounts for design speed, radius and superelevation rate was developed to overcome the discrepancies in the Green Book (Bonneson, 2001). However, it is unclear if this method has been adopted by any agency.



What does all this mean for NCDOT? Since 1933 when the State Highway Commission was created, there have been construction efforts to pave unpaved roads and construct new roads to get the citizens of the state out of the mud. Design standards have evolved over time, with slight variations as each new version of the AASHTO Green Book is published. When the need arises, an engineer's field investigation that checks horizontal curvature against superelevation must be based on sound engineering principles that meet current design standards.

#### Crash Reconstruction

A primary application of a field procedure for identifying and investigating horizontal curves with insufficient superelevation rates is crash reconstruction. The National Cooperative Highway Research Program (NCHRP) Synthesis 369 is a valuable resource of the practices of state DOT crash reconstruction (NCHRP 369, 2007). NCHRP Synthesis 369 provides a state of the practice summary of the involvement and procedures of state departments of transportation in crash reconstruction. The researchers utilized a survey, local technical assistance inquires, and website searches to acquire the pertinent information.

The research found that about 26% (11 of 43) of the DOTs are routinely involved in crash reconstruction with a designated unit or consultant<sup>1</sup>. Other DOTs reported that consultants were utilized in response to lawsuits. The number of employees involved in the crash reconstructions varied from one to eight across the survey respondents. In some court cases, expert witnesses were hired by state DOTs that had designated units. Reconstructions were conducted immediately after the incident, or months or years later in some cases.

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<sup>&</sup>lt;sup>1</sup> California, Delaware, Kansas, Kentucky, Louisiana, New Mexico, Nevada, North Carolina, Oklahoma, Pennsylvania, and, West Virginia



#### RECOMMENDED CURVE INVESTIGATION METHOD

The research team visited nine curve locations in Wake County to observe the variability of curve characteristics and understand the limitations of investigation applications. The procedures were developed with field condition considerations for the parameters of radius, superelevation, and stopping sight distance. The eight-step procedure is fully contained in Appendix A along with the Field Investigation Form. The aim of the procedure was to be time and cost-efficient for implementation by a single person.

Of particular interest during the initial trials is the finding that a 50' chord length was the easiest to use in the field. It provided a long enough length to measure a middle ordinate for some longer radii, while still being very manageable in stretching out the tape to get it taught. Other chord lengths tried included 30' and 40' lengths, but these were generally felt to be too short unless the radius was small, say under 200 feet.

The following steps, including the overall categories shown in Exhibit 8 (General Study, Radius and Superelevation, Stopping Sight Distance, and Engineering Judgment), will provide the procedural steps and the conceptual or computational background for the completion of the field investigation for each of the curve characteristics of interest.

The first two steps are general guidelines for following appropriate safety precautions and the proper equipment needed for the study (step 1) and general curve investigation guidelines (step 2). The radius is a key parameter for describing a curve and for comparisons to standard design guidelines. The radius can be determined by using a chord that is within the curve limits and the corresponding middle ordinate value of the chord. The superelevation of the curve is used to compare the radius to AASHTO design recommendations. Four steps provide the instructions for the investigation of curve radius and superelevation. Step 3 details the method for determining the middle ordinate distance. Step 4 describes the method for determining the superelevation of the curve. Step 5 provides the information for converting the middle ordinate distance into a radius value. Step 6 determines the AASHTO minimum recommended radius which can be



compared to the field measured value. Step 7 provides the investigator with a method to determine if stopping sight distance is a concern through the horizontal curve. Step 8 provides concluding information about the study procedure and the importance of engineering judgment.

General Study
Step 1: Safety and Equipment
Step 2: General Curve Investigation

Radius and Superelevation
Step 3: Measurement of Middle Ordinate
Step 4: Measurement of Superelevation
Step 5: Radius Determination
Step 6: AASHTO Minimum Radius Determination

Step 7: Stopping Sight Distance
Step 7: Stopping Sight Distance Determination

**Exhibit 8: Curve Investigation Method** 

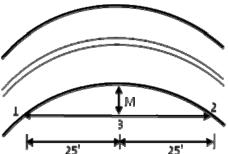
1. Safety and Equipment – Before beginning any field investigation, check that all equipment is available and operable. Although this procedure was developed to minimize exposure to vehicles, some interaction is necessary, so follow NCDOT guidelines for personal safety while implementing this field procedure. Necessary equipment includes:

Step 8: Engineering Judgment

- a. Safety Vest (Class II or above as required)
- b. Digital Level (4' long)
- c. Hammer
- d. Masonry Nails (e.g., Parker-Kalon 1½" by ¼")
- e. Measuring Tape (50' or 100' Metal or Cloth, with metal preferred)
- f. Metal Tape Measure (25')
- g. Clipboard, Field Investigation Form, and Pen
- h. Three Orange Traffic Cones (2' tall)
- i. Measuring Wheel



- 2. General Curve Investigation Determine the limits (Point of Curvature, PC, and Point of Tangency, PT) of the curve through visual observations of the tangent sections leading into and out of the curve. All measurements should occur within these limits of the curve. Try to locate representative areas of the curve to conduct your measurements, avoiding any abnormalities. The first measurement should be about in the middle of the curve.
- 3. Measurement of Middle Ordinate Determine the middle ordinate measurement through the following steps:
  - a. Place nails in the pavement on the outside edge of the edgeline stripping 50' apart (at points 1 and 2 in Exhibit 9). One nail can be used to hold the hook at the end of the 50' measuring tape and the second nail can be used to pull the tape against or around (if cloth tape is used). The tape must be pulled taught and remain straight for step 3b.
  - b. Measure the middle ordinate distance at the middle point of the tape (25'), using the smaller tape measure (at point 3 in the figure). The distance M should be read and recorded to the nearest 1/8".
  - c. Repeat this measurement by moving points 1 and 2 together about 10 feet left and then 10 feet right of the first measurement. This provides three measurements.

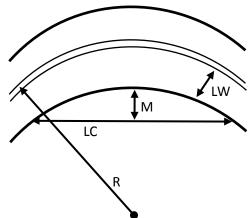


**Exhibit 9: Middle Ordinate Measurement** 

- 4. Measurement of Superelevation Determine the superelevation of the curve by measuring the superelevation of the roadway perpendicular to the direction of travel by reading and recording five measurements that are representative of the superelevation of the middle section of the curve in each lane. Circle the median value, which will be used as the superelevation value. This value must be in increments of 0.2% as represented in the AASHTO Minimum Radius Tables. If necessary, round the field measured value up or down to the nearest 0.2% increment.
- 5. Radius Determination Determine the radius of the curve by using the circled middle ordinate value from the Field Investigation Form and the Middle Ordinate Conversion Table (Exhibit 11). Add the inside lane width to the table value to determine the centerline radius of the curve. Record the value on the Field Investigation Form. Exhibit 10 provides a visual display of the parameters used to determine the radius.



**Exhibit 10: Curve Radius Determination** 



$$R = \frac{M^2 + 0.25LC^2}{2M} + LW$$

Where:

R = Radius (feet)

M = Middle Ordinate (feet)

LW = Lane Width (feet)

LC = Long Chord (feet)

**Exhibit 11: Middle Ordinate Conversion Table** 

| EXHIBIT 1                     | Exhibit 11: Middle Ordinate Conversion Table |                               |   |                               |   |                               |   |  |  |
|-------------------------------|--|-------------------------------|---|-------------------------------|---|-------------------------------|---|--|--|
|                               | Middle Ordinate Conversion Table             |                               |   |                               |   |                               |   |  |  |
| Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft  | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft |  |  |
| 0.125                         | 30,000                                       | 2.625                         | 1,429                                       | 5.25                          | 715   | 10.25                         | 366   |  |  |
| 0.250                         | 15,000                                       | 2.750                         | 1,364                                       | 5.50                          | 682   | 10.50                         | 358   |  |  |
| 0.375                         | 10,000                                       | 2.875                         | 1,304                                       | 5.75                          | 652   | 10.75                         | 349   |  |  |
| 0.500                         | 7,500  | 3.000                         | 1,250                                       | 6.00                          | 625   | 11.00                         | 341   |  |  |
| 0.625                         | 6,000  | 3.125                         | 1,200                                       | 6.25                          | 600   | 11.25                         | 334   |  |  |
| 0.750                         | 5,000  | 3.250                         | 1,154                                       | 6.50                          | 577   | 11.50                         | 327   |  |  |
| 0.875                         | 4,286  | 3.375                         | 1,111                                       | 6.75                          | 556   | 11.75                         | 320   |  |  |
| 1.000                         | 3,750  | 3.500                         | 1,072                                       | 7.00                          | 536   | 12.00                         | 313   |  |  |
| 1.125                         | 3,333  | 3.625                         | 1,035                                       | 7.25                          | 518   | 12.25                         | 307   |  |  |
| 1.250                         | 3,000  | 3.750                         | 1,000                                       | 7.50                          | 500   | 12.50                         | 301   |  |  |
| 1.375                         | 2,727  | 3.875                         | 968   | 7.75                          | 484   | 12.75                         | 295   |  |  |
| 1.500                         | 2,500  | 4.000                         | 938   | 8.00                          | 469   | 13.00                         | 289   |  |  |
| 1.625                         | 2,308  | 4.125                         | 909   | 8.25                          | 455   | 13.25                         | 284   |  |  |
| 1.750                         | 2,143  | 4.250                         | 883   | 8.50                          | 442   | 13.50                         | 278   |  |  |
| 1.875                         | 2,000  | 4.375                         | 857   | 8.75                          | 429   | 13.75                         | 273   |  |  |
| 2.000                         | 1,875  | 4.500                         | 834   | 9.00                          | 417   | 14.00                         | 268   |  |  |
| 2.125                         | 1,765  | 4.625                         | 811   | 9.25                          | 406   | 14.25                         | 264   |  |  |
| 2.250                         | 1,667  | 4.750                         | 790   | 9.50                          | 395   | 14.50                         | 259   |  |  |
| 2.375                         | 1,579  | 4.875                         |   | 9.75                          | 385   | 14.75                         | 255   |  |  |
| 2.500                         | 1,500  | 5.000                         | 750   | 10.00                         | 375   | 15.00                         | 251   |  |  |

Note: Add inside lane width to radius value from table to find centerline radius for a two-lane highway.

6. AASHTO Minimum Radius Determination – Determine the minimum recommended radius of the curve by using the circled superelevation value from the Field Investigation Form and the appropriate AASHTO Minimum Radius Table (for an e<sub>max</sub> of 4%, 6%, or 8%). Record the value on the Field Investigation Form. The AASHTO Minimum Radius for the inside lane and outside lane will be equal if the superelevations for each lane are equal.



The selection of the appropriate  $e_{max}$  value is important. Shoulder sections of two-lane roadways should have a design superelevation of 8% for higher speed segments or 6% for lower speed segments. The comparison can be examined for both design superelevations, if necessary. A design superelevation of 4% should be used for curb and gutter sections of urban roadways. Additional maximum superelevation rate guidance is available from the NCDOT Roadway Design Manual – Part 1, Chapter 1: General Design.

Exhibit 12: AASHTO Minimum Radius Table  $(e_{max} = 4\%)$ 

| AASHTO Minimum Radius Table (e <sub>max</sub> = 4%) |       |          |               |                      |       |  |
|---|-------|----------|---------------|----------------------|-------|--|
|   |       | Posted S | peed Limit, ' | V <sub>d</sub> (mph) |       |  |
| Superelevation, e (%)                               | 35    | 40       | 45            | 50                   | 55    |  |
|   |       |          | Radius (ft)   |                      |       |  |
| 1.5   | 3,730 | 4,770    | 5,930         | 7,220                | 8,650 |  |
| 2.0   | 2,490 | 3,220    | 4,040         | 4,940                | 5,950 |  |
| 2.2   | 2,120 | 2,760    | 3,480         | 4,280                | 5,180 |  |
| 2.4   | 1,760 | 2,340    | 2,980         | 3,690                | 4,500 |  |
| 2.6   | 1,420 | 1,930    | 2,490         | 3,130                | 3,870 |  |
| 2.8   | 1,170 | 1,620    | 2,100         | 2,660                | 3,310 |  |
| 3.0   | 982   | 1,370    | 1,800         | 2,290                | 2,860 |  |
| 3.2   | 835   | 1,180    | 1,550         | 1,980                | 2,490 |  |
| 3.4   | 714   | 1,010    | 1,340         | 1,720                | 2,170 |  |
| 3.6   | 610   | 865      | 1,150         | 1,480                | 1,880 |  |
| 3.8   | 512   | 730      | 970           | 1,260                | 1,600 |  |
| 4.0   | 371   | 533      | 711           | 926                  | 1,190 |  |



**Exhibit 13: AASHTO Minimum Radius Table (e<sub>max</sub> = 6%)** 

| AASHTO Minimum Radius Table (e <sub>max</sub> = 6%) |  |       |             |       |       |  |
|---|--|-------|-------------|-------|-------|--|
|   | Posted Speed Limit, V <sub>d</sub> (mph) |       |             |       |       |  |
| Superelevation, e (%)                               | 35                                       | 40    | 45          | 50    | 55    |  |
|   |  |       | Radius (ft) |       |       |  |
| 1.5   | 4,100                                    | 5,230 | 6,480       | 7,870 | 9,410 |  |
| 2.0   | 2,950                                    | 3,770 | 4,680       | 5,700 | 6,820 |  |
| 2.2   | 2,630                                    | 3,370 | 4,190       | 5,100 | 6,110 |  |
| 2.4   | 2,360                                    | 3,030 | 3,770       | 4,600 | 5,520 |  |
| 2.6   | 2,130                                    | 2,740 | 3,420       | 4,170 | 5,020 |  |
| 2.8   | 1,930                                    | 2,490 | 3,110       | 3,800 | 4,580 |  |
| 3.0   | 1,760                                    | 2,270 | 2,840       | 3,480 | 4,200 |  |
| 3.2   | 1,600                                    | 2,080 | 2,600       | 3,200 | 3,860 |  |
| 3.4   | 1,460                                    | 1,900 | 2,390       | 2,940 | 3,560 |  |
| 3.6   | 1,320                                    | 1,740 | 2,190       | 2,710 | 3,290 |  |
| 3.8   | 1,190                                    | 1,590 | 2,010       | 2,490 | 3,040 |  |
| 4.0   | 1,070                                    | 1,440 | 1,840       | 2,300 | 2,810 |  |
| 4.2   | 960                                      | 1,310 | 1,680       | 2,110 | 2,590 |  |
| 4.4   | 868                                      | 1,190 | 1,540       | 1,940 | 2,400 |  |
| 4.6   | 788                                      | 1,090 | 1,410       | 1,780 | 2,210 |  |
| 4.8   | 718                                      | 995   | 1,300       | 1,640 | 2,050 |  |
| 5.0   | 654                                      | 911   | 1,190       | 1,510 | 1,890 |  |
| 5.2   | 595                                      | 833   | 1,090       | 1,390 | 1,750 |  |
| 5.4   | 540                                      | 759   | 995         | 1,280 | 1,610 |  |
| 5.6   | 487                                      | 687   | 903         | 1,160 | 1,470 |  |
| 5.8   | 431                                      | 611   | 806         | 1,040 | 1,320 |  |
| 6.0   | 340                                      | 485   | 643         | 833   | 1,060 |  |

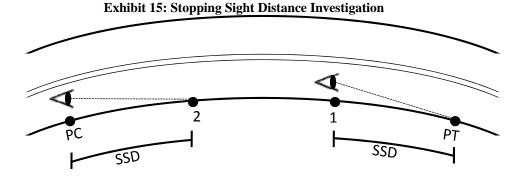


Exhibit 14: AASHTO Minimum Radius Table ( $e_{max} = 8\%$ )

|  | Exhibit 14: AASHTO Minimum Radius Table $(e_{max} = 8\%)$ AASHTO Minimum Radius Table $(e_{max} = 8\%)$ |       |       |       |       |  |  |
|--|---|-------|-------|-------|-------|--|--|
| Posted Speed Limit, V <sub>d</sub> (mph) |   |       |       |       |       |  |  |
| Superelevation, e (%)                    | 35 40 45 50   |       |       |       | 55    |  |  |
|  | Radius (ft)   |       |       |       |       |  |  |
| 1.5                                      | 4,260   | 5,410 | 6,710 | 8,150 | 9,720 |  |  |
| 2.0                                      | 3,120   | 3,970 | 4,930 | 5,990 | 7,150 |  |  |
| 2.2                                      | 2,800   | 3,570 | 4,440 | 5,400 | 6,450 |  |  |
| 2.4                                      | 2,540   | 3,240 | 4,030 | 4,910 | 5,870 |  |  |
| 2.6                                      | 2,320   | 2,960 | 3,690 | 4,490 | 5,370 |  |  |
| 2.8                                      | 2,130   | 2,720 | 3,390 | 4,130 | 4,950 |  |  |
| 3.0                                      | 1,960   | 2,510 | 3,130 | 3,820 | 4,580 |  |  |
| 3.2                                      | 1,820   | 2,330 | 2,900 | 3,550 | 4,250 |  |  |
| 3.4                                      | 1,690   | 2,170 | 2,700 | 3,300 | 3,970 |  |  |
| 3.6                                      | 1,570   | 2,020 | 2,520 | 3,090 | 3,710 |  |  |
| 3.8                                      | 1,470   | 1,890 | 2,360 | 2,890 | 3,480 |  |  |
| 4.0                                      | 1,370   | 1,770 | 2,220 | 2,720 | 3,270 |  |  |
| 4.2                                      | 1,280   | 1,660 | 2,080 | 2,560 | 3,080 |  |  |
| 4.4                                      | 1,200   | 1,560 | 1,960 | 2,410 | 2,910 |  |  |
| 4.6                                      | 1,130   | 1,470 | 1,850 | 2,280 | 2,750 |  |  |
| 4.8                                      | 1,060   | 1,390 | 1,750 | 2,160 | 2,610 |  |  |
| 5.0                                      | 991   | 1,310 | 1,650 | 2,040 | 2,470 |  |  |
| 5.2                                      | 929   | 1,230 | 1,560 | 1,930 | 2,350 |  |  |
| 5.4                                      | 870   | 1,160 | 1,480 | 1,830 | 2,230 |  |  |
| 5.6                                      | 813   | 1,090 | 1,390 | 1,740 | 2,120 |  |  |
| 5.8                                      | 761   | 1,030 | 1,320 | 1,650 | 2,010 |  |  |
| 6.0                                      | 713   | 965   | 1,250 | 1,560 | 1,920 |  |  |
| 6.2                                      | 669   | 909   | 1,180 | 1,480 | 1,820 |  |  |
| 6.4                                      | 628   | 857   | 1,110 | 1,400 | 1,730 |  |  |
| 6.6                                      | 590   | 808   | 1,050 | 1,330 | 1,650 |  |  |
| 6.8                                      | 553   | 761   | 990   | 1,260 | 1,560 |  |  |
| 7.0                                      | 518   | 716   | 933   | 1,190 | 1,480 |  |  |
| 7.2                                      | 485   | 672   | 878   | 1,120 | 1,400 |  |  |
| 7.4                                      | 451   | 628   | 822   | 1,060 | 1,320 |  |  |
| 7.6                                      | 417   | 583   | 765   | 980   | 1,230 |  |  |
| 7.8                                      | 380   | 533   | 701   | 901   | 1,140 |  |  |
| 8.0                                      | 314   | 444   | 587   | 758   | 960   |  |  |



- 7. Stopping Sight Distance (SSD) Determination Estimate whether or not the curve provides SSD through the following steps:
  - a. Determine the AASHTO Minimum SSD which is found in the AASHTO Minimum Stopping Sight Distance Table (Exhibit 16).
  - b. Place one orange traffic cone at the PT of the curve on the edge of the roadway. If a second person is present, that person can temporarily place the traffic cone in the center of the lane during step 7d. However, the edge of the roadway is an appropriate approximation.
  - c. Using the measuring wheel, roll out the AASHTO Minimum SSD distance along the edgeline of the roadway towards the PC of the curve (point 1 in Exhibit 15).
  - d. At the AASHTO Minimum SSD distance, look back and record whether or not the traffic cone is visible. It is helpful to step into the middle of the inside lane and stoop down so that your eye height is about 3.5' above the pavement.
  - e. Next, place another orange traffic cone at the PC of the curve to mark the location.
  - f. Using the measuring wheel, roll out the AASHTO Minimum SSD distance along the edgeline of the roadway towards the PT of the curve and place the third orange traffic cone (point 2 in Exhibit 15) at the edge of the roadway. If a second person is present, that person can temporarily place the traffic cone in the center of the lane during step 7g. However, the edge of the roadway is an appropriate approximation.
  - g. Return to the PC of the curve, look back and record whether or not the traffic cone is visible. It is helpful to step into the middle of the inside lane and stoop down so that your eye height is about 3.5' above the pavement.
  - h. If the traffic cone is visible from both locations (PC to 2, and 1 to PT), SSD is provided through the curve unless an obstruction close to the ditch line is present near the center of the curve.
  - i. If the traffic cone (2 or PT) is not visible from either location (PC or 1), SSD is not provided through the curve.





**Exhibit 16: AASHTO Minimum Stopping Sight Distance** 

| AASHTO Minimum Stopping Sight Distance Table |  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|--|
| Minimum SSD (ft)                             |  |  |  |  |  |  |  |
| 80   |  |  |  |  |  |  |  |
| 115  |  |  |  |  |  |  |  |
| 155  |  |  |  |  |  |  |  |
| 200  |  |  |  |  |  |  |  |
| 250  |  |  |  |  |  |  |  |
| 305  |  |  |  |  |  |  |  |
| 360  |  |  |  |  |  |  |  |
| 425  |  |  |  |  |  |  |  |
| 495  |  |  |  |  |  |  |  |
| 570  |  |  |  |  |  |  |  |
| 645  |  |  |  |  |  |  |  |
| 730  |  |  |  |  |  |  |  |
| 820  |  |  |  |  |  |  |  |
| 910  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

Source: AASHTO A Policy on Geometric Design of Highways and Streets 2004

8. Engineering Judgment – This simple field procedure is aimed at determining mitigation factors for the parameters of radius, superelevation, and stopping sight distance. The field measured radius, superelevation, and stopping sight distance are compared to AASHTO recommended values. Engineering judgment is needed to determine appropriate action based on these measurements and comparisons.



#### **SUMMARY**

This research effort aimed to develop a simple procedure using measurement devices readily available that a single engineer can use to determine the radius and superelevation of any horizontal curve. The measurements taken can be applied against a chart to determine the radius. Then, with the superelevation measurement, a determination is made if the curve radius and superelevation meet current design standards for the posted speed limit for the highway. The horizontal SSD can also be checked against current design standards as well, again by only one engineer. Thus, superelevation, radius, and horizontal SSD can be checked against current design standards.

In addition to documenting the field procedure through a MS PowerPoint® presentation, the research team put together a recorded, self-playing presentation using Elluminate *Publish!*® Both the PowerPoint® and self-playing presentations were provided to NCDOT for their future use in training staff on this procedure.



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- NCHRP 369. (2007). State DOT Crash Reconstruction Practices A Synthesis of Highway Practice. Washington, DC: Transportation Research Board.



# **APPENDIX A: CURVE INVESTIGATION PROCEDURE**

# **Field Investigation Procedure**

## **Simple Field Procedure for Determining Horizontal Curve Radius**

Developed Under NCDOT Research Project 2009-09

by

Robert S. Foyle, P.E.

and

Daniel J. Findley, E.I.

at the

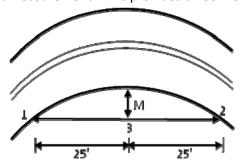
Institute for Transportation Research and Education
North Carolina State University

Raleigh, North Carolina

May 31, 2009

#### **Simple Field Procedure for Determining Horizontal Curve Radius**

- 1. Safety and Equipment Before beginning any field investigation, check that all equipment is available and operable. Although this procedure was developed to minimize exposure to vehicles, some interaction is necessary, so follow NCDOT guidelines for personal safety while implementing this field procedure. Necessary equipment includes:
  - a. Safety Vest (Class II or above as required)
  - b. Digital Level (4' long)
  - c. Hammer
  - d. Masonry Nails (e.g., Parker-Kalon 1½" by ¼")
  - e. Measuring Tape (50' or 100' Metal or Cloth, with metal preferred)
  - f. Metal Tape Measure (25')
  - g. Clipboard, Field Investigation Form, and Pen
  - h. Three Orange Traffic Cones (2' tall)
  - i. Measuring Wheel
- 2. General Curve Investigation Determine the limits (Point of Curvature, PC, and Point of Tangency, PT) of the curve through visual observations of the tangent sections leading into and out of the curve. All measurements should occur within these limits of the curve. Try to locate representative areas of the curve to conduct your measurements, avoiding any abnormalities. The first measurement should be about in the middle of the curve.
- 3. Measurement of Middle Ordinate Determine the middle ordinate measurement through the following steps:
  - a. Place nails in the pavement on the outside edge of the edgeline stripping 50' apart (at points 1 and 2 in the figure). One nail can be used to hold the hook at the end of the 50' measuring tape and the second nail can be used to pull the tape against or around (if cloth tape is used). The tape must be pulled taught and remain straight for step 3b.
  - b. Measure the middle ordinate distance at the middle point of the tape (25'), using the smaller tape measure (at point 3 in the figure). The distance M should be read and recorded to the nearest 1/8".
  - c. Repeat this measurement by moving points 1 and 2 together about 10 feet left and then 10 feet right of the first measurement. This provides three measurements.





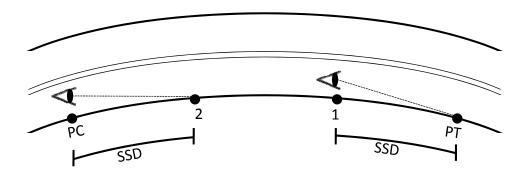
- 4. Measurement of Superelevation Determine the superelevation of the curve by measuring the superelevation of the roadway perpendicular to the direction of travel by reading and recording five measurements that are representative of the superelevation of the middle section of the curve in each lane. Circle the median value, which will be used as the superelevation value. This value must be in increments of 0.2% as represented in the AASHTO Minimum Radius Tables. If necessary, round the field measured value up or down to the nearest 0.2% increment.
- 5. Radius Determination Determine the radius of the curve by using the circled middle ordinate value from the Field Investigation Form and the Middle Ordinate Conversion Table. Add the inside lane width to the table value to determine the centerline radius of the curve. Record the value on the Field Investigation Form.
- 6. AASHTO Minimum Radius Determination Determine the minimum recommended radius of the curve by using the circled superelevation value from the Field Investigation Form and the appropriate AASHTO Minimum Radius Table (for an  $e_{max}$  of either 4%, 6%, or 8%). Record the value on the Field Investigation Form. The AASHTO Minimum Radius for the inside lane and outside lane will be equal if the superelevations for each lane are equal.

The selection of the appropriate  $e_{max}$  value is important. Shoulder sections of two-lane roadways should have a design superelevation of 8% for higher speed segments or 6% for lower speed segments. The comparison can be examined for both design superelevations, if necessary. A design superelevation of 4% should be used for curb and gutter sections of urban roadways. Additional maximum superelevation rate guidance is available from the NCDOT Roadway Design Manual – Part 1, Chapter 1: General Design.

- 7. Stopping Sight Distance (SSD) Determination Estimate whether or not the curve provides SSD through the following steps:
  - a. Determine the AASHTO Minimum SSD which is found in the AASHTO Minimum Stopping Sight Distance Table.
  - b. Place one orange traffic cone at the PT of the curve on the edge of the roadway. If a second person is present, that person can temporarily place the traffic cone in the center of the lane during step 7d. However, the edge of the roadway is an appropriate approximation.
  - c. Using the measuring wheel, roll out the AASHTO Minimum SSD distance along the edgeline of the roadway towards the PC of the curve (point 1 in the figure).
  - d. At the AASHTO Minimum SSD distance, look back and record whether or not the traffic cone is visible. It is helpful to step into the middle of the inside lane and stoop down so that your eye height is about 3.5' above the pavement.
  - e. Next, place another orange traffic cone at the PC of the curve to mark the location.
  - f. Using the measuring wheel, roll out the AASHTO Minimum SSD distance along the edgeline of the roadway towards the PT of the curve and place the third orange traffic



- cone (point 2 in the figure) at the edge of the roadway. If a second person is present, that person can temporarily place the traffic cone in the center of the lane during step 7g. However, the edge of the roadway is an appropriate approximation.
- g. Return to the PC of the curve, look back and record whether or not the traffic cone is visible. It is helpful to step into the middle of the inside lane and stoop down so that your eye height is about 3.5' above the pavement.
- h. If the traffic cone is visible from both locations (PC to 2, and 1 to PT), SSD is provided through the curve unless an obstruction close to the ditch line is present near the center of the curve.
- i. If the traffic cone (2 or PT) is not visible from either location (PC or 1), SSD is not provided through the curve.



8. Engineering Judgment – This simple field procedure is aimed at determining mitigation factors for the parameters of radius, superelevation, and stopping sight distance. The field measured radius, superelevation, and stopping sight distance are compared to AASHTO recommended values. Engineering judgment is needed to determine appropriate action based on these measurements and comparisons.



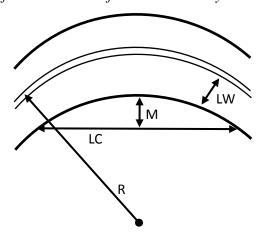
|   |          |               | Fiel       | d Investigation F                      | orm      |                       |                     |   |
|---|----------|---------------|------------|--|----------|-----------------------|---------------------|---|
| Investigator:                             |          |               |            |  |          |                       |                     |   |
| Date:                                     |          |               |            |  |          |                       |                     |   |
| Location:                                 |          |               |            |  |          |                       |                     |   |
| Posted Speed Limit:                       | :        |               |            |  |          |                       |                     |   |
|   |          |               | Middl      | e Ordinate Measure                     | ments    |                       |                     |   |
| Measurem                                  | ent 1:   |               |            | Measurement 2:                         |          | Meas                  | surement 3:         |   |
|   |          |               |            |  |          |                       |                     |   |
|   |          | inches        |            |  | inches   |                       | inches              | 5 |
|   |          |               |            | ld be used as the mi                   |          |                       |                     |   |
| Middle Ordinate Co                        | nversio  | n Table       | e to de    | termine the radius.                    | Record   | the radius val        | ue below.           | _ |
| Radius:                                   |          |               |            |  |          |                       |                     |   |
|   |          | Insid         | de Lane    | Superelevation Mea                     | asurem   | ents                  |                     | - |
| Measurement 1:                            | Mea      | sureme        | ent 2:     | Measurement 3:                         | Mea      | surement 4:           | Measurement 5:      | - |
| 0/  |          |               | %          | %                                      |          | 0/                    | %                   |   |
| %   |          |               | 70         | 70                                     | %        |                       | 70                  |   |
|   |          | Outs          | ide Lan    | e Superelevation Me                    | easuren  | nents                 |                     |   |
| Measurement 1:                            | Mea      | easurement 2: |            | Measurement 3:                         | Mea      | surement 4:           | Measurement 5:      |   |
| %   |          |               | %          | %                                      |          | %                     | %                   |   |
|   |          |               |            |  |          |                       |                     |   |
|   |          |               |            | side and outside lane                  |          |                       |                     |   |
|   |          |               |            | HTO Radius Table to                    |          |                       |                     |   |
| both lanes.                               | max allu | record        | i tile ili | inimum radius value                    | 2 DEIOW  | v baseu on the        | s superelevation of |   |
|   | .1. 0    | Insid         | e Lane     | AASHTO Minimum F                       | Radius.  | R::                   | _                   | _ |
| e <sub>max</sub> : 4.0% (for co           |          |               |            | e AASHTO Minimum                       |          |                       |                     | _ |
| 6.0% (for l                               |          |               |            |  |          |                       |                     | _ |
| e <sub>max</sub> : speed show             |          |               |            | AASHTO Minimum F                       |          |                       |                     | _ |
| segmen                                    |          | Outs          | ide Lan    | e AASHTO Minimum                       | n Radiu: | s, R <sub>min</sub> : |                     |   |
| 8.0% (for h e <sub>max</sub> : speed show | -        | Insid         | e Lane     | AASHTO Minimum F                       | Radius,  | R <sub>min</sub> :    |                     |   |
| segmen                                    |          | Outs          | ide Lan    | e AASHTO Minimum                       | n Radiu  | s, R <sub>min</sub> : |                     |   |
|   |          | Sto           | opping     | Sight Distance Meas                    | ureme    | nts                   |                     |   |
| AASHTO Minin                              | num SSI  | D:            |            | visible at PC from                     |          | Yes                   | No                  |   |
|   |          |               |            | O Minimum SSD?                         |          |                       |                     | _ |
|   |          | feet          |            | e visible at PT from<br>O Minimum SSD? |          | Yes                   | No                  |   |
| Circle the appropria                      | te resp  |               |            | visibility from the P                  | C and P  | T. Use the AA         | ASHTO Minimum       | - |
| Stopping Sight Dista                      | ance Tal | ble to d      | determ     | ine the AASHTO Min                     | imum S   | SSD.                  |                     |   |
|   |          |               |            | Notes                                  |          |                       |                     | _ |
|   |          |               |            |  |          |                       |                     |   |



| Middle Ordinate Conversion Table |   |                               |   |                               |   |                               |   |  |  |
|----------------------------------|---|-------------------------------|---|-------------------------------|---|-------------------------------|---|--|--|
| Middle<br>Ordinate,<br>M (in)    | Radius (ft) for a<br>Long Chord of<br>50 ft | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft | Middle<br>Ordinate,<br>M (in) | Radius (ft) for a<br>Long Chord of<br>50 ft |  |  |
| 0.125                            | 30,000                                      | 2.625                         | 1,429                                       | 5.25                          | 715   | 10.25                         | 366   |  |  |
| 0.250                            | 15,000                                      | 2.750                         | 1,364                                       | 5.50                          | 682   | 10.50                         | 358   |  |  |
| 0.375                            | 10,000                                      | 2.875                         | 1,304                                       | 5.75                          | 652   | 10.75                         | 349   |  |  |
| 0.500                            | 7,500                                       | 3.000                         | 1,250                                       | 6.00                          | 625   | 11.00                         | 341   |  |  |
| 0.625                            | 6,000                                       | 3.125                         | 1,200                                       | 6.25                          | 600   | 11.25                         | 334   |  |  |
| 0.750                            | 5,000                                       | 3.250                         | 1,154                                       | 6.50                          | 577   | 11.50                         | 327   |  |  |
| 0.875                            | 4,286                                       | 3.375                         | 1,111                                       | 6.75                          | 556   | 11.75                         | 320   |  |  |
| 1.000                            | 3,750                                       | 3.500                         | 1,072                                       | 7.00                          | 536   | 12.00                         | 313   |  |  |
| 1.125                            | 3,333                                       | 3.625                         | 1,035                                       | 7.25                          | 518   | 12.25                         | 307   |  |  |
| 1.250                            | 3,000                                       | 3.750                         | 1,000                                       | 7.50                          | 500   | 12.50                         | 301   |  |  |
| 1.375                            | 2,727                                       | 3.875                         | 968   | 7.75                          | 484   | 12.75                         | 295   |  |  |
| 1.500                            | 2,500                                       | 4.000                         | 938   | 8.00                          | 469   | 13.00                         | 289   |  |  |
| 1.625                            | 2,308                                       | 4.125                         | 909   | 8.25                          | 455   | 13.25                         | 284   |  |  |
| 1.750                            | 2,143                                       | 4.250                         | 883   | 8.50                          | 442   | 13.50                         | 278   |  |  |
| 1.875                            | 2,000                                       | 4.375                         | 857   | 8.75                          | 429   | 13.75                         | 273   |  |  |
| 2.000                            | 1,875                                       | 4.500                         | 834   | 9.00                          | 417   | 14.00                         | 268   |  |  |
| 2.125                            | 1,765                                       | 4.625                         | 811   | 9.25                          | 406   | 14.25                         | 264   |  |  |
| 2.250                            | 1,667                                       | 4.750                         | 790   | 9.50                          | 395   | 14.50                         | 259   |  |  |
| 2.375                            | 1,579                                       | 4.875                         | 769   | 9.75                          | 385   | 14.75                         | 255   |  |  |
| 2.500                            | 1,500                                       | 5.000                         | 750   | 10.00                         | 375   | 15.00                         | 251   |  |  |

Note: Add inside lane width to radius value from table to find centerline radius for a two-lane highway.

To find the radius of a curve with any chord length, the following equation can be used:



$$R = \frac{M^2 + 0.25LC^2}{2M} + LW$$

Where:

R = Radius (feet)

M = Middle Ordinate (feet)

LW = Lane Width (feet)

LC = Long Chord (feet)



| AASHTO Minimum Radius Table (e <sub>max</sub> = 4%) |  |       |             |       |       |  |  |
|---|--|-------|-------------|-------|-------|--|--|
|   | Posted Speed Limit, V <sub>d</sub> (mph) |       |             |       |       |  |  |
| Superelevation, e (%)                               | 35                                       | 40    | 45          | 50    | 55    |  |  |
|   |  |       | Radius (ft) |       |       |  |  |
| 1.5   | 3,730                                    | 4,770 | 5,930       | 7,220 | 8,650 |  |  |
| 2.0   | 2,490                                    | 3,220 | 4,040       | 4,940 | 5,950 |  |  |
| 2.2   | 2,120                                    | 2,760 | 3,480       | 4,280 | 5,180 |  |  |
| 2.4   | 1,760                                    | 2,340 | 2,980       | 3,690 | 4,500 |  |  |
| 2.6   | 1,420                                    | 1,930 | 2,490       | 3,130 | 3,870 |  |  |
| 2.8   | 1,170                                    | 1,620 | 2,100       | 2,660 | 3,310 |  |  |
| 3.0   | 982                                      | 1,370 | 1,800       | 2,290 | 2,860 |  |  |
| 3.2   | 835                                      | 1,180 | 1,550       | 1,980 | 2,490 |  |  |
| 3.4   | 714                                      | 1,010 | 1,340       | 1,720 | 2,170 |  |  |
| 3.6   | 610                                      | 865   | 1,150       | 1,480 | 1,880 |  |  |
| 3.8   | 512                                      | 730   | 970         | 1,260 | 1,600 |  |  |
| 4.0   | 371                                      | 533   | 711         | 926   | 1,190 |  |  |



| AASHTO Minimum Radius Table (e <sub>max</sub> = 6%) |  |          |             |       |       |  |  |
|---|--|----------|-------------|-------|-------|--|--|
|   | Posted Speed Limit, V <sub>d</sub> (mph) |          |             |       |       |  |  |
| Superelevation, e (%)                               | 35                                       | 35 40 45 |             | 50    | 55    |  |  |
|   |  |          | Radius (ft) |       |       |  |  |
| 1.5   | 4,100                                    | 5,230    | 6,480       | 7,870 | 9,410 |  |  |
| 2.0   | 2,950                                    | 3,770    | 4,680       | 5,700 | 6,820 |  |  |
| 2.2   | 2,630                                    | 3,370    | 4,190       | 5,100 | 6,110 |  |  |
| 2.4   | 2,360                                    | 3,030    | 3,770       | 4,600 | 5,520 |  |  |
| 2.6   | 2,130                                    | 2,740    | 3,420       | 4,170 | 5,020 |  |  |
| 2.8   | 1,930                                    | 2,490    | 3,110       | 3,800 | 4,580 |  |  |
| 3.0   | 1,760                                    | 2,270    | 2,840       | 3,480 | 4,200 |  |  |
| 3.2   | 1,600                                    | 2,080    | 2,600       | 3,200 | 3,860 |  |  |
| 3.4   | 1,460                                    | 1,900    | 2,390       | 2,940 | 3,560 |  |  |
| 3.6   | 1,320                                    | 1,740    | 2,190       | 2,710 | 3,290 |  |  |
| 3.8   | 1,190                                    | 1,590    | 2,010       | 2,490 | 3,040 |  |  |
| 4.0   | 1,070                                    | 1,440    | 1,840       | 2,300 | 2,810 |  |  |
| 4.2   | 960                                      | 1,310    | 1,680       | 2,110 | 2,590 |  |  |
| 4.4   | 868                                      | 1,190    | 1,540       | 1,940 | 2,400 |  |  |
| 4.6   | 788                                      | 1,090    | 1,410       | 1,780 | 2,210 |  |  |
| 4.8   | 718                                      | 995      | 1,300       | 1,640 | 2,050 |  |  |
| 5.0   | 654                                      | 911      | 1,190       | 1,510 | 1,890 |  |  |
| 5.2   | 595                                      | 833      | 1,090       | 1,390 | 1,750 |  |  |
| 5.4   | 540                                      | 759      | 995         | 1,280 | 1,610 |  |  |
| 5.6   | 487                                      | 687      | 903         | 1,160 | 1,470 |  |  |
| 5.8   | 431                                      | 611      | 806         | 1,040 | 1,320 |  |  |
| 6.0   | 340                                      | 485      | 643         | 833   | 1,060 |  |  |



| AASHTO Minimum Radius Table (e <sub>max</sub> = 8%) |  |       |       |       |       |  |  |  |
|---|--|-------|-------|-------|-------|--|--|--|
|   | Posted Speed Limit, V <sub>d</sub> (mph) |       |       |       |       |  |  |  |
| Superelevation, e (%)                               | 35                                       | 40    | 40 45 |       | 55    |  |  |  |
|   | 35 40 45 50 55<br>Radius (ft)            |       |       |       |       |  |  |  |
| 1.5   | 4,260                                    | 5,410 | 6,710 | 8,150 | 9,720 |  |  |  |
| 2.0   | 3,120                                    | 3,970 | 4,930 | 5,990 | 7,150 |  |  |  |
| 2.2   | 2,800                                    | 3,570 | 4,440 | 5,400 | 6,450 |  |  |  |
| 2.4   | 2,540                                    | 3,240 | 4,030 | 4,910 | 5,870 |  |  |  |
| 2.6   | 2,320                                    | 2,960 | 3,690 | 4,490 | 5,370 |  |  |  |
| 2.8   | 2,130                                    | 2,720 | 3,390 | 4,130 | 4,950 |  |  |  |
| 3.0   | 1,960                                    | 2,510 | 3,130 | 3,820 | 4,580 |  |  |  |
| 3.2   | 1,820                                    | 2,330 | 2,900 | 3,550 | 4,250 |  |  |  |
| 3.4   | 1,690                                    | 2,170 | 2,700 | 3,300 | 3,970 |  |  |  |
| 3.6   | 1,570                                    | 2,020 | 2,520 | 3,090 | 3,710 |  |  |  |
| 3.8   | 1,470                                    | 1,890 | 2,360 | 2,890 | 3,480 |  |  |  |
| 4.0   | 1,370                                    | 1,770 | 2,220 | 2,720 | 3,270 |  |  |  |
| 4.2   | 1,280                                    | 1,660 | 2,080 | 2,560 | 3,080 |  |  |  |
| 4.4   | 1,200                                    | 1,560 | 1,960 | 2,410 | 2,910 |  |  |  |
| 4.6   | 1,130                                    | 1,470 | 1,850 | 2,280 | 2,750 |  |  |  |
| 4.8   | 1,060                                    | 1,390 | 1,750 | 2,160 | 2,610 |  |  |  |
| 5.0   | 991                                      | 1,310 | 1,650 | 2,040 | 2,470 |  |  |  |
| 5.2   | 929                                      | 1,230 | 1,560 | 1,930 | 2,350 |  |  |  |
| 5.4   | 870                                      | 1,160 | 1,480 | 1,830 | 2,230 |  |  |  |
| 5.6   | 813                                      | 1,090 | 1,390 | 1,740 | 2,120 |  |  |  |
| 5.8   | 761                                      | 1,030 | 1,320 | 1,650 | 2,010 |  |  |  |
| 6.0   | 713                                      | 965   | 1,250 | 1,560 | 1,920 |  |  |  |
| 6.2   | 669                                      | 909   | 1,180 | 1,480 | 1,820 |  |  |  |
| 6.4   | 628                                      | 857   | 1,110 | 1,400 | 1,730 |  |  |  |
| 6.6   | 590                                      | 808   | 1,050 | 1,330 | 1,650 |  |  |  |
| 6.8   | 553                                      | 761   | 990   | 1,260 | 1,560 |  |  |  |
| 7.0   | 518                                      | 716   | 933   | 1,190 | 1,480 |  |  |  |
| 7.2   | 485                                      | 672   | 878   | 1,120 | 1,400 |  |  |  |
| 7.4   | 451                                      | 628   | 822   | 1,060 | 1,320 |  |  |  |
| 7.6   | 417                                      | 583   | 765   | 980   | 1,230 |  |  |  |
| 7.8   | 380                                      | 533   | 701   | 901   | 1,140 |  |  |  |
| 8.0   | 314                                      | 444   | 587   | 758   | 960   |  |  |  |



| AASHTO Minimum Stopping Sight Distance Table |                  |  |  |  |  |  |  |
|--|------------------|--|--|--|--|--|--|
| Speed Limit (mph)                            | Minimum SSD (ft) |  |  |  |  |  |  |
| 15   | 80               |  |  |  |  |  |  |
| 20   | 115              |  |  |  |  |  |  |
| 25   | 155              |  |  |  |  |  |  |
| 30   | 200              |  |  |  |  |  |  |
| 35   | 250              |  |  |  |  |  |  |
| 40   | 305              |  |  |  |  |  |  |
| 45   | 360              |  |  |  |  |  |  |
| 50   | 425              |  |  |  |  |  |  |
| 55   | 495              |  |  |  |  |  |  |
| 60   | 570              |  |  |  |  |  |  |
| 65   | 645              |  |  |  |  |  |  |
| 70   | 730              |  |  |  |  |  |  |
| 75   | 820              |  |  |  |  |  |  |
| 80   | 910              |  |  |  |  |  |  |





## APPENDIX B: CURVE INVESTIGATION EXAMPLE



|  | Fie            | ld Investigation Fo   | orm     |                       |                |  |  |  |
|--|----------------|---|---------|-----------------------|----------------|--|--|--|
| Investigator: Johr   | n Smith        |   |         |                       |                |  |  |  |
| Date: 2/11/2009  |                |   |         |                       |                |  |  |  |
|  |                |   |         |                       |                |  |  |  |
| Posted Speed Limit:  | 45 MPH         |   | /       |                       |                |  |  |  |
| '  |                | le Ordinate Measure   | ments   |                       |                |  |  |  |
| Measurement 1:   |                | Measurement 2:  |         | Mea                   | surement 3:    |  |  |  |
| 8 1/8  | inches 8       | * 4   | inches  | 9 <sup>5</sup> /      | 8 inches       |  |  |  |
| Circle the median value at<br>Middle Ordinate Conversion   |                |   |         |                       |                |  |  |  |
| Radius:  |                | 455' + 10' (Lar   |         | ,                     | j'             |  |  |  |
| Magazina   |                | Superelevation Mea  |         |                       | Magazina       |  |  |  |
| Measurement 1: Mea   | surement 2:    | Measurement 3:  | iviea   | surement 4:           | Measurement 5: |  |  |  |
| 8.2 %  | 8.0 %          | 8.4 %   |         | 8.4 %                 | 8.0 %          |  |  |  |
|  |                | e Superelevation Me   |         |                       |                |  |  |  |
| Measurement 1: Mea   | surement 2:    | Measurement 3:  | Mea     | surement 4:           | Measurement 5: |  |  |  |
| 8.0 %  | 7.8 %          | 7.8 %   |         | 7.6 %                 | 7.8 %          |  |  |  |
| Circle the median value at superelevation measurem radius. Select the e <sub>max</sub> and both lanes. | ent in the AAS | SHTO Radius Table to  | detern  | nine the AASH         | ITO minimum    |  |  |  |
| 4.0% (for curb &   | Inside Lane    | AASHTO Minimum F  | Radius, | R <sub>min</sub> :    |                |  |  |  |
| e <sub>max</sub> : gutter segments)  | Outside La     | ne AASHTO Minimum   | Radius  | s, R <sub>min</sub> : |                |  |  |  |
| 6.0% (for lower  | Inside Lane    | AASHTO Minimum F  | Radius, | R <sub>min</sub> :    |                |  |  |  |
| e <sub>max</sub> : speed shoulder  |                | ne AASHTO Minimum   |         |                       |                |  |  |  |
| 8.0% (for higher   |                | AASHTO Minimum F  |         |                       | 587'           |  |  |  |
| e <sub>ma</sub> : speed shoulder segments)   | Outside Lai    | Outside Lane AASHTO Minimum Radius, R <sub>min</sub> : 701' |         |                       |                |  |  |  |
| segmentsj  | Stopping       | Sight Distance Meas   | uremei  | nts                   |                |  |  |  |
| AASHTO Minimum SS  |                | e visible from PC to  |         | Yes                   | No             |  |  |  |
| 260  | -              | TO Minimum SSD?   |         | 103                   |                |  |  |  |
| 360 Is cone visible at PT from AASHTO Minimum SSD?  No   |                |   |         |                       | No             |  |  |  |
| Circle the appropriate response for cone visibility from the PC and to the PT. Use the AASHTO          |                |   |         |                       |                |  |  |  |
| Minimum Stopping Sight Distance Table to determine the AASHTO Minimum SSD.                             |                |   |         |                       |                |  |  |  |
| Notes  |                |   |         |                       |                |  |  |  |
| Existing curve radius < Rmin and SSD sight line check failed on  |                |   |         |                       |                |  |  |  |
| both ends of the cu  | rve.           |   |         |                       |                |  |  |  |