

# LRFD FOUNDATION DESIGN FOR FLYOVER 13 OVER I-95 AND I-73

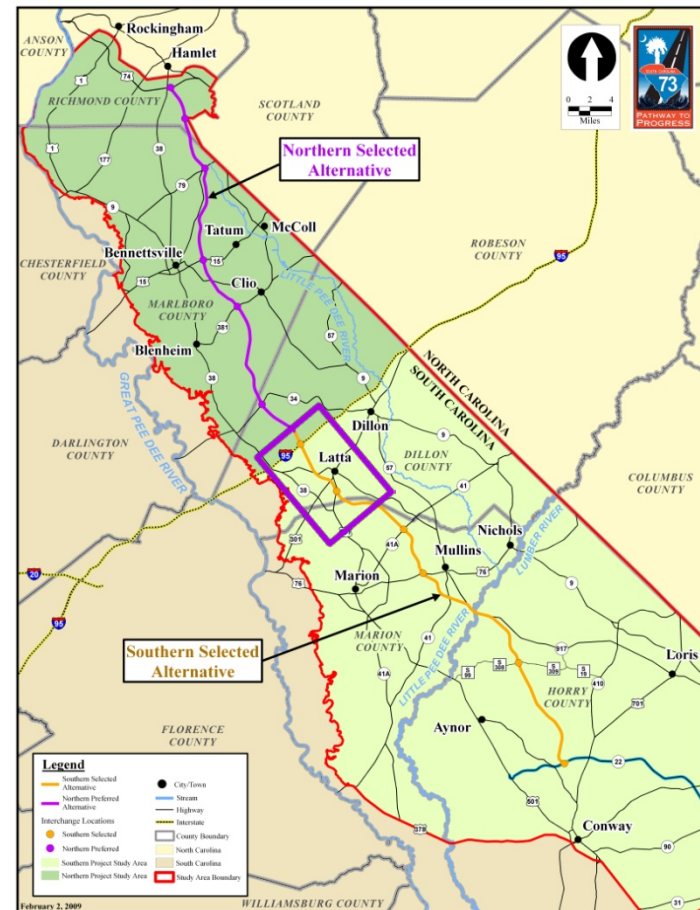


Sanjoy Chakraborty  
PhD, PE

April 4, 2013  
Geo<sup>3</sup> T<sup>2</sup> Conference

# I-73 Phase 1 Overview

- I-95 to US-501
- \$166 Million Construction Cost
- About 5.7 mi of Interstate Hwy.
- 10 Bridges
- Partial Interchange at I-95



# Bridge 4B Design

- Ramp from I-95 South to I-73 South
- Crossing over I-95 and I-73
- 2,514 ft. in length
- 8 spans
- Post-tensioned concrete segmental box girder
- Hammerhead piers on drilled shaft groups
- Steel piles at abutments

# Geotechnical Design Procedure

- Geotechnical Exploration and Laboratory Testing
- Conduct Site Response Analysis
  - Design Acceleration Response Spectra
  - Design Acceleration Time History Data Sets
  - Analysis of Seismic Hazards
- Design of Bridge Foundations
- Design of Embankments and Retaining Walls
- Foundation Substructure Analysis
  - Dynamic Stiffness and Damping compatible with Superstructure Model

# Geotechnical Exploration

- Preliminary (Right-of-way) Phase
  - 5 SPT borings
  - Seismic CPT soundings
  - Deep boring to 500 feet with shear wave velocity measurements
- Final (Construction Plans) Phase
  - Borings at abutments and interior bents
  - Borings at approach embankments and MSE wall locations
- Laboratory Testing

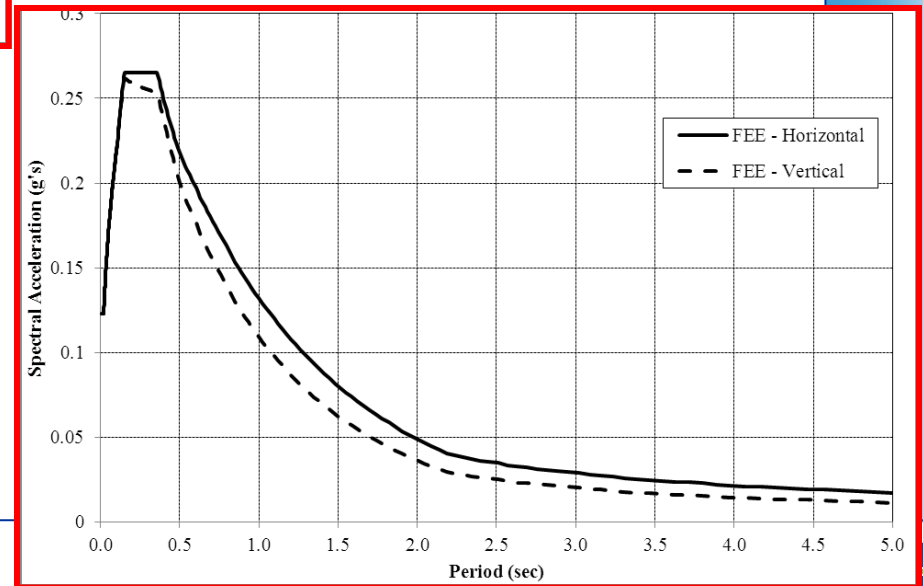
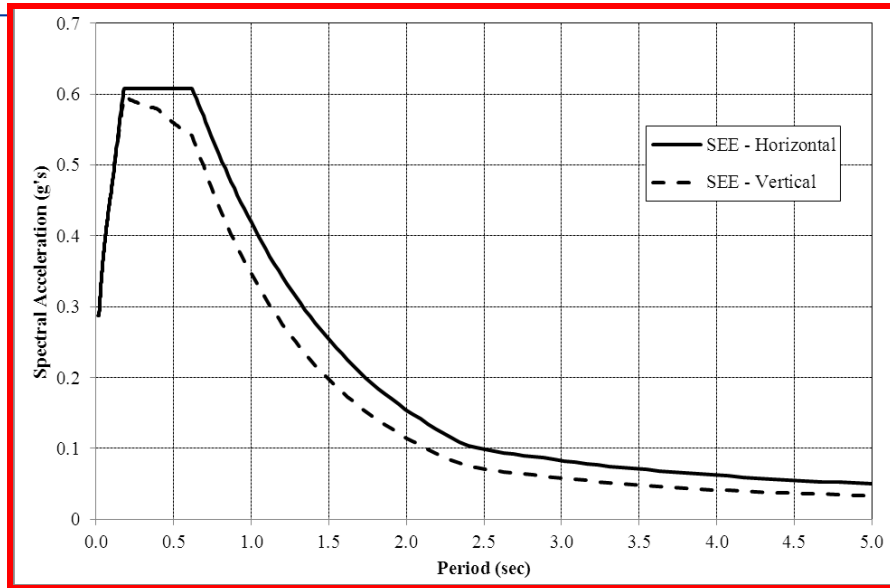
# Subsurface Conditions

- 25 to 40 feet of Pleistocene soils
  - Sands with clay and silt
  - Measured SPT from WOH to 26
- 10 to 25 feet of Bear Bluff soils
  - Sands with clay and silt, some fat clay
  - Measured SPT from 3 to 28
- Black Creek soils to bottom of borings
  - Sands and silty sands, low plasticity fines, some cementation
  - Measured SPT from 5 to 86

# Site Response Analysis

- SEE and FEE Design Scenarios
- SHAKE Analysis – South Carolina Soils
- Development of site specific Acceleration Response Spectra
  - Horizontal
  - Vertical
- Development of spatially incoherent and spectrum compatible acceleration time histories for SEE
  - 3 sets total
  - Horizontal and vertical components
  - Developed at support locations (abutments and interior bents)

# Design Response Spectra : 5% Damping





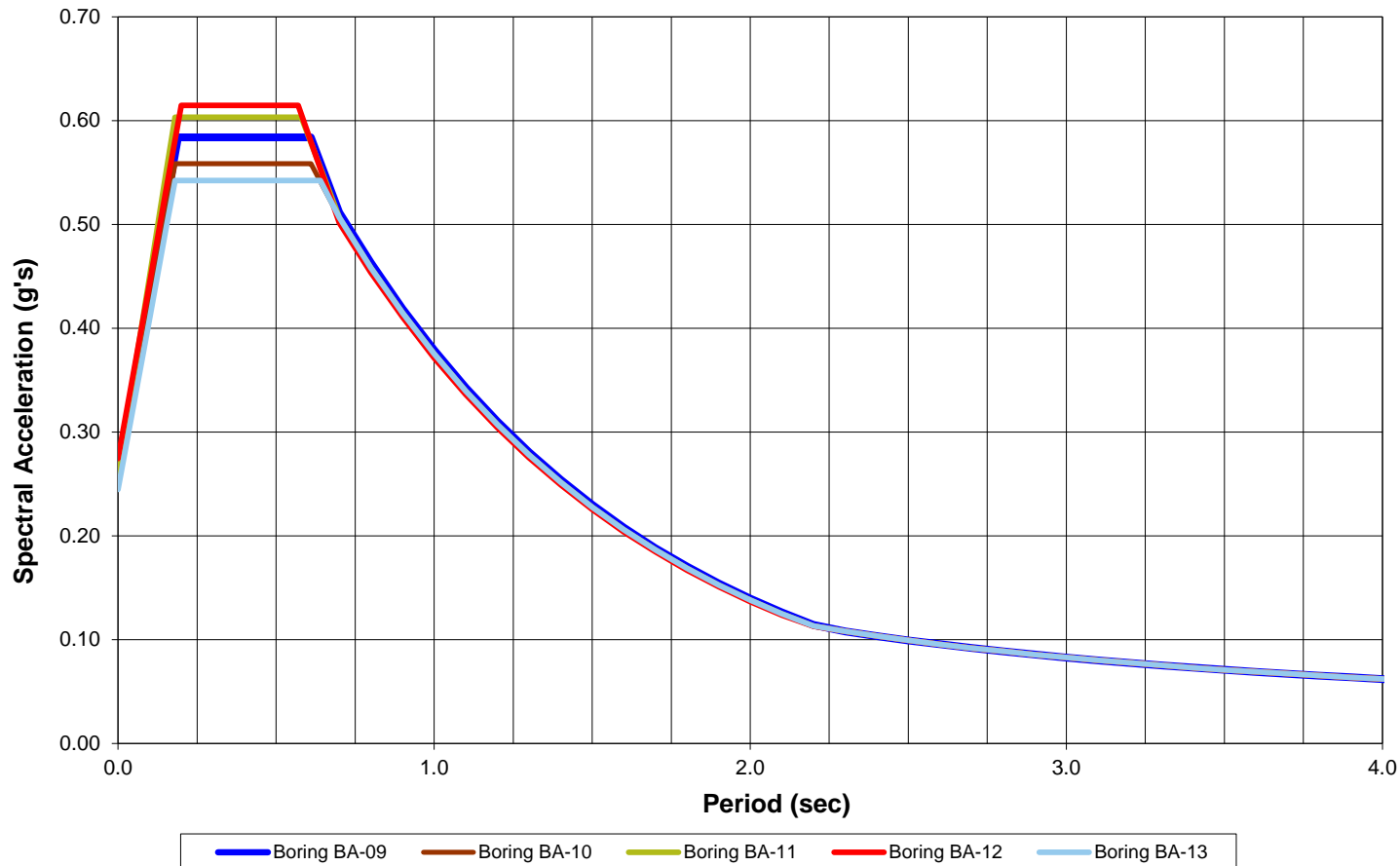
# Site Response Analysis

## Development of Spectrum Compatible Horizontal and Vertical Acceleration Time Histories

- Variability – subsurface conditions
- Spatial variability of motion – wave passage effects
- Incoherency of motion

# Subsurface Variability

Design Horizontal Acceleration Response Spectra at GROUND SURFACE  
Damping = 5 %



# Wave Passage Effects

- Spatial Variability of Motion
- Incoherency of Motion

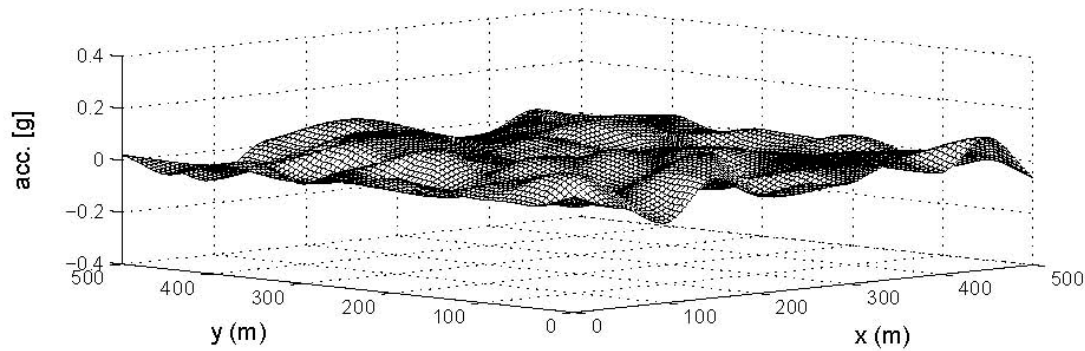
# Spatial Variability



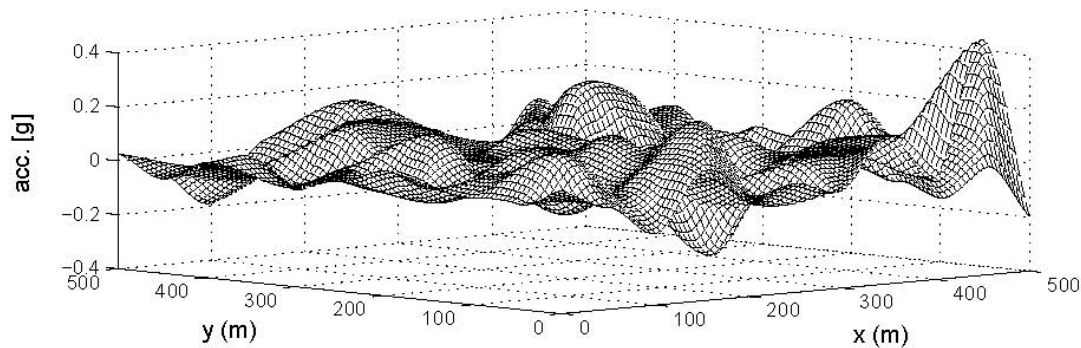
# Incoherency of Motions

Inhomogeneous soil, USGS soil types A,C  $t=2$  sec

(a) Gaussian ground accelerations at  $t = 2$  sec



(b) Non-Gaussian ground accelerations at  $t = 2$  sec



# Seismic Hazards

- Idriss and Boulanger, 2008 Monograph + SCDOT GDM
- Site Specific Demands from SHAKE (CSR)
- Liquefaction and Cyclic Softening
- Seismically Induced Settlements
- Horizontal Movements
- Residual Shear Strengths
- Downdrag loads
- Mitigation at abutments – earthquake drains

# Design of Bridge Foundations

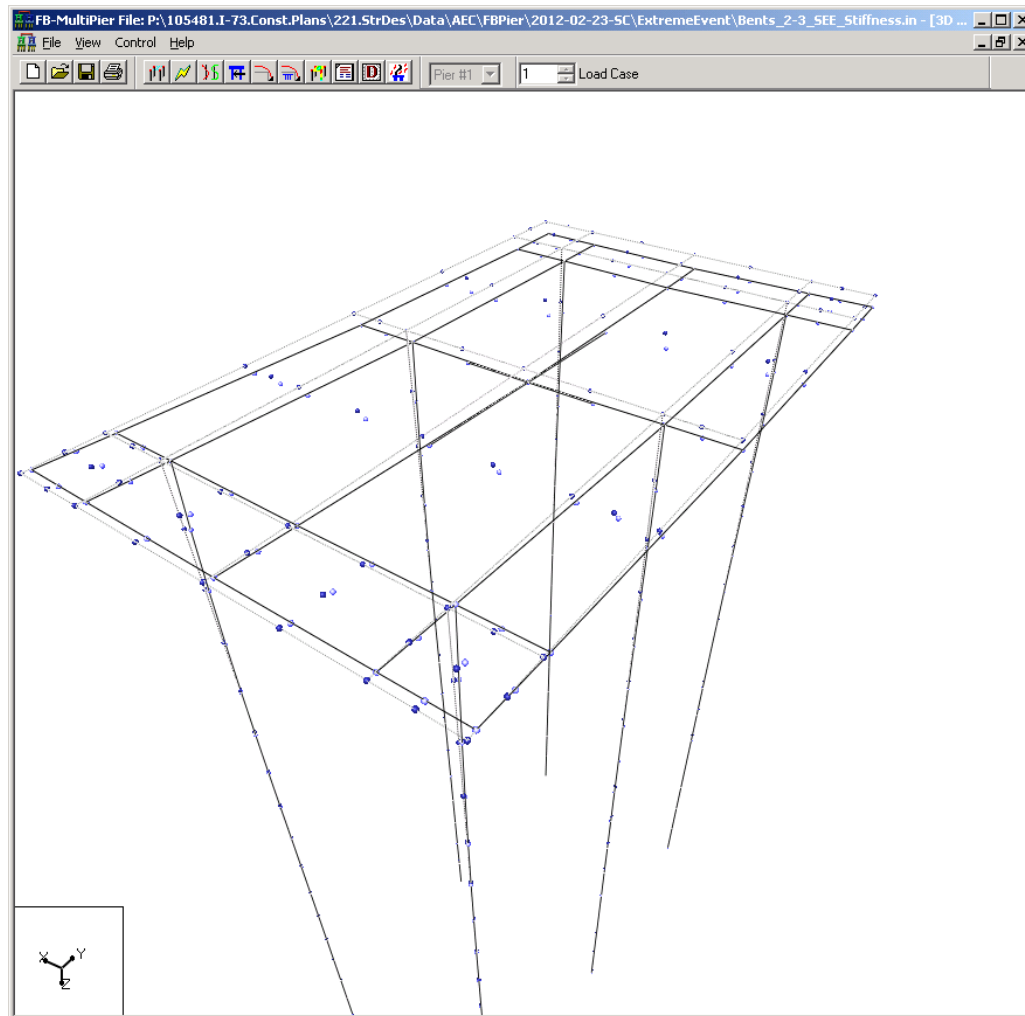
- AASHTO LRFD 2010 + SCDOT GDM
- Driven pile group at abutments
- Drilled shaft group at interior bents
- Limit States
  - Service
  - Strength
  - Construction (Strength)
  - Extreme Event

# Design of Bridge Foundations

- Group analysis using FB-Multiplier
  - Movements : Service
  - Shaft demands : Strength and Extreme Event
  - Equivalent linear stiffness – compatible with superstructure analyses
  
- Shaft axial resistance
  - AASHTO + SCDOT Resistance Factors
  - Load test data
  - Group effects
  - Downdrag from seismic settlements

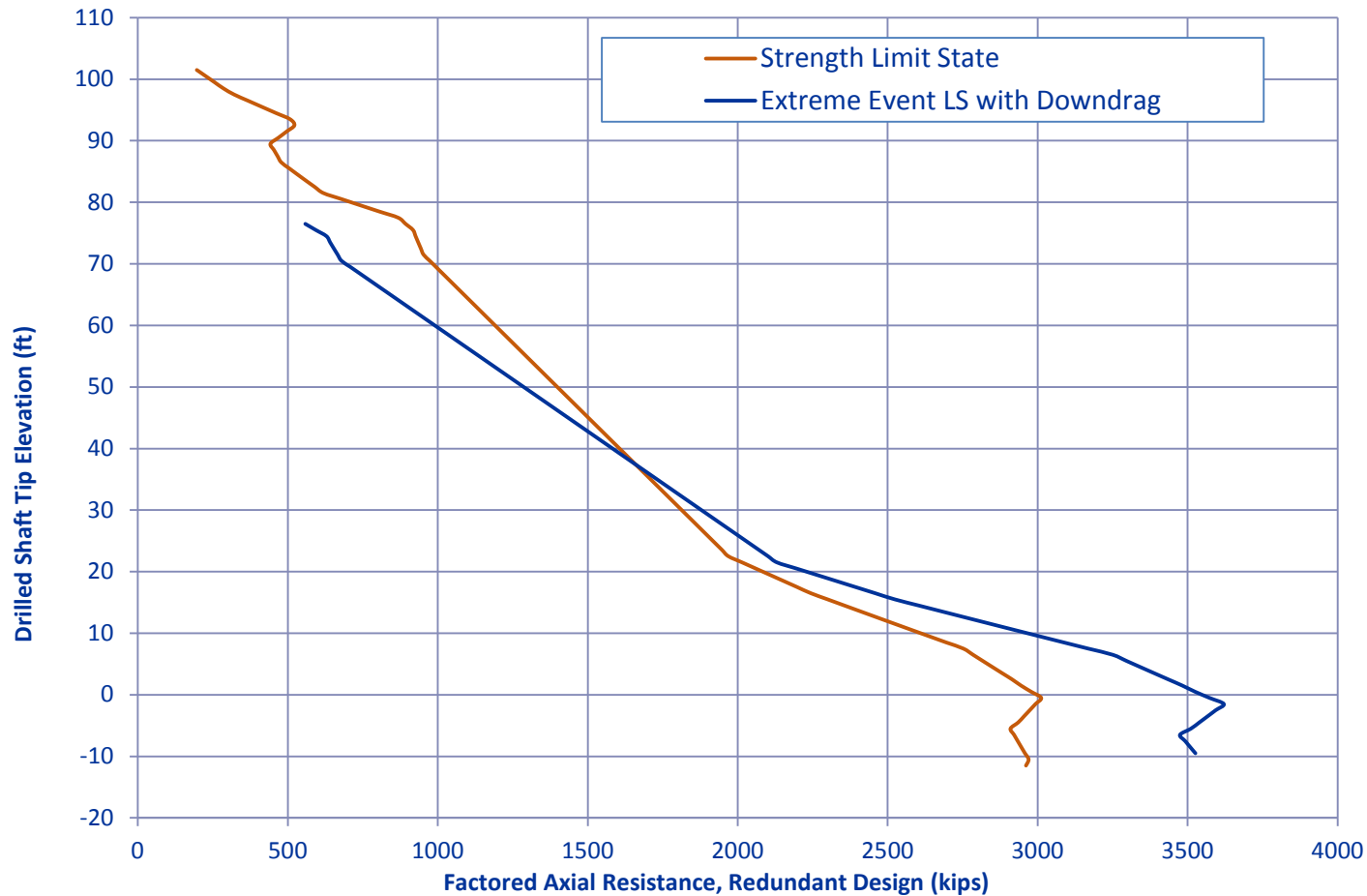


# FB-Multiplier Models



# Shaft Axial Resistance – Bent 4

Diameter = 7.0-ft



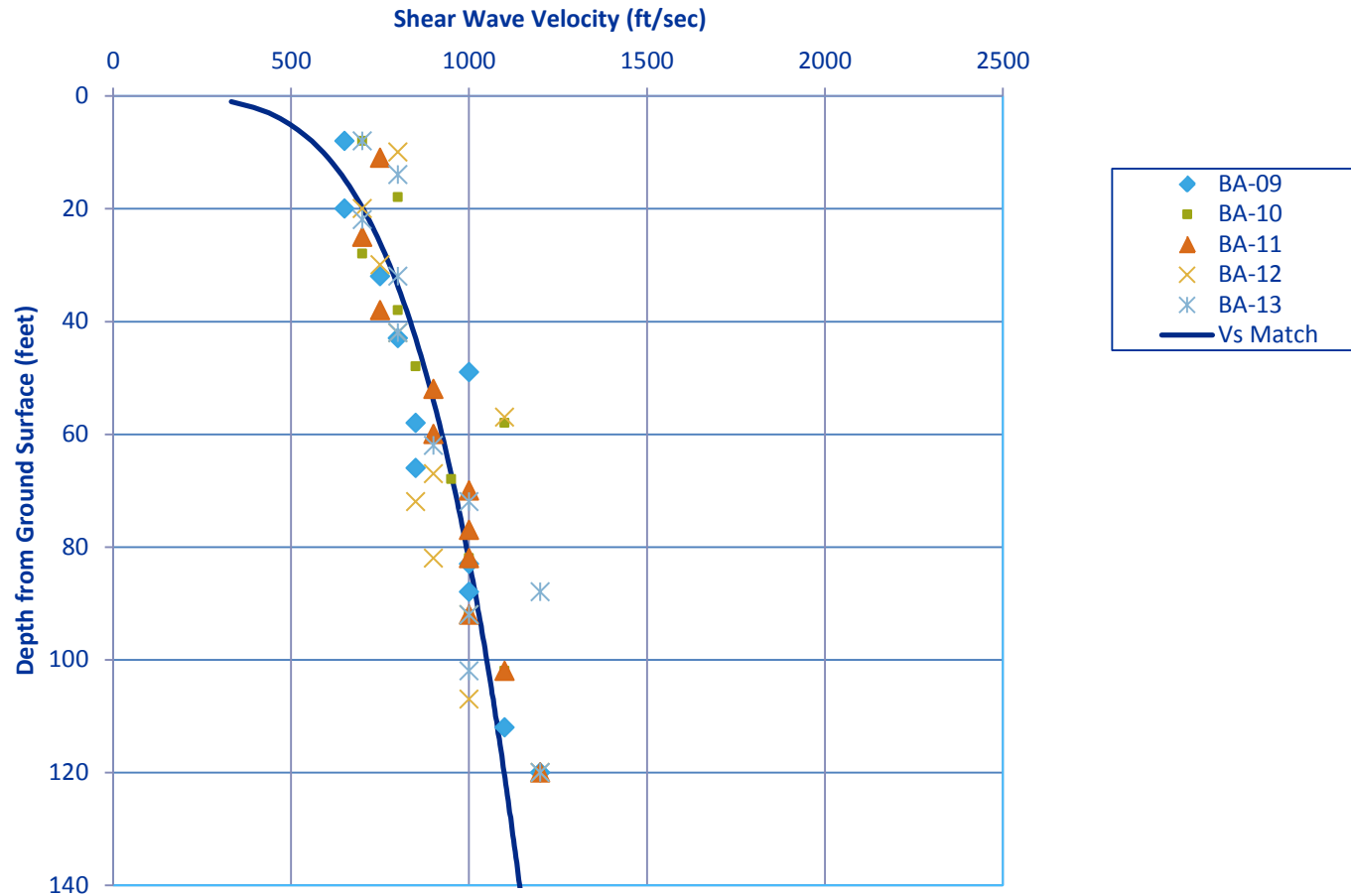
# Drilled Shaft Design

Bent	Strength Limit State		Extreme Event Limit State : SEE			
	Maximum Factored Load (kips)		Minimum Tip Elevation - Strength (ft)	Maximum Factored Load (kips)	Minimum Tip Elevation EE (ft)	Required Minimum Tip Elevation (ft)
	Construction	Strength				
<b>2</b>	2,406	2,545	<b>6</b>	2,570	9	<b>6</b>
<b>3</b>	2,406	2,545	<b>15</b>	2,570	18	<b>15</b>
<b>4</b>	2,518	2,939	0	3,681	-6	<b>-6</b>
<b>5</b>	2,518	2,939	9	3,681	12	<b>9</b>
<b>6</b>	2,518	2,939	<b>-3</b>	3,681	-3	<b>-3</b>
<b>7</b>	2,390	2,484	9	2,603	40	<b>9</b>
<b>8</b>	2,390	2,484	<b>17</b>	2,603	42	<b>17</b>

# Foundation Model for Time History Analysis

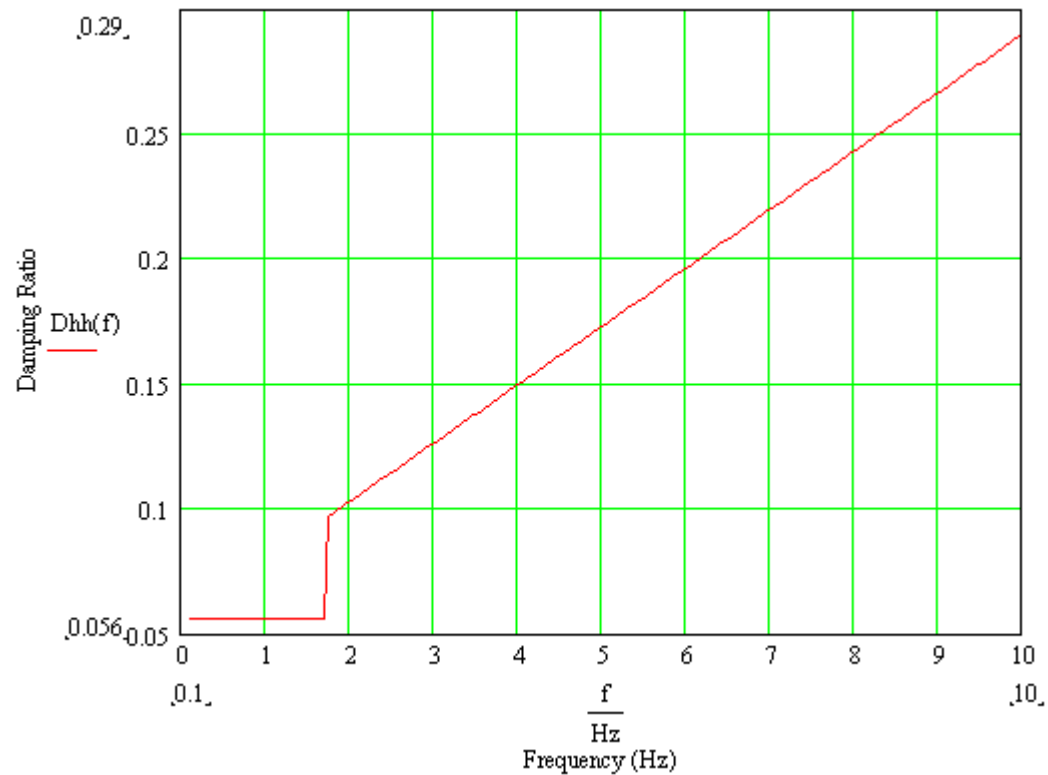
- Equivalent static stiffness for SEE loads
  - 6x6 stiffness matrix for group
  - Iterations for compatibility
- Frequency dependent damping
  - Shear wave velocity/Shear Modulus profile
  - Frequency dependent damping ratio/dashpots
  - Horizontal, rocking, vertical and cross-coupling terms

# Shear Wave Velocity Model

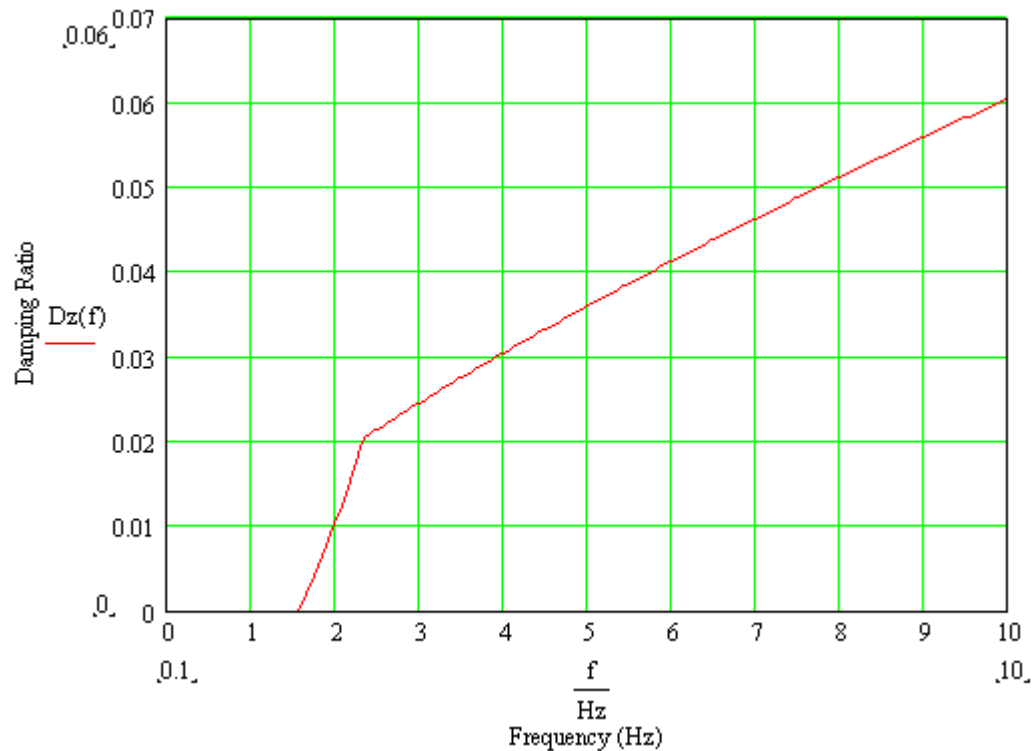


Shear Wave Velocity Model based on SHAKE site-specific analyses models

# Shaft Head Damping – Lateral Swaying



# Shaft Head Damping – Vertical (Axial)



# Seismic Analysis of Superstructure

- Michael Baker Corp. and CDM Smith
  - Response Spectrum
  - Pushover
  - Time History
- Multiple iterations to achieve compatibility between substructure and superstructure models



# I-73/I-95 Interchange Bridge 4B

- Questions?